

# The `xypdf` package

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## Abstract

The `xypdf` package improves the output quality of the `Xy-pic` package when PDF documents are generated. It produces generic PDF code for graphical elements like lines, curves and circles instead of approximating these elements with glyphs in special fonts as the original `Xy-pic` package does. The `xypdf` package works both with pdf $\LaTeX$  and the two-step compilation  $\LaTeX \rightarrow \text{dvi} \rightarrow \text{pdf}$ .

## 1 Introduction

The `Xy-pic` package is a utility for typesetting diagrams in  $\TeX$  and  $\LaTeX$  documents. The authors of the `Xy-pic` package put much effort into the feature that most graphical elements are coded within the limited possibilities of the device independent file format (DVI) and can thus be generated with even the most basic  $\TeX$  systems and displayed universally by all device drivers. For example, diagonal lines are composed of short dashes, which are glyphs in a special font. Since there are dashes in 127 discrete directions in the font `xydash10`, diagonal lines which do not match one of these slopes look slightly rugged when they are magnified.

For a better output quality in Postscript files, the authors of the `Xy-pic` package provided a Postscript backend for DVI-to-Postscript drivers. These extensions draw lines and curves by generic Postscript commands, thus trading a much better output quality against universality of the produced DVI files.

As the most recent version 3.7 of `Xy-pic` dates from 1999, there is no support for pdf $\TeX$ . In order to produce PDF files with high-quality `Xy-pic` diagrams, users had to use so far the Postscript file format as an intermediate step or embed the diagrams as external graphics. However, since many users directly generate PDF files from the  $\TeX$  or DVI files (with bookmarks, hyperlinks and other PDF features), it is highly desirable to also have the possibility of directly generating `Xy-pic` diagrams with high-quality PDF graphics elements.

The present package `xypdf` adapts the output routines of the `Xy-pic` package to generate high-quality graphics for PDF output. It works with both pdf $\LaTeX$  and the two-step compilation  $\LaTeX \rightarrow \text{dvi} \rightarrow \text{pdf}$  with an intermediate DVI file. Note that some version of  $\epsilon\text{-}\TeX$  is needed (which is anyway used by default in modern  $\TeX$  installations). Figure 1 compares the output quality of a small `Xy-pic` figure.

The `xypdf` package is very similar to the Postscript backend to `Xy-pic`. It does not have (yet) all features of the Postscript backend (see Section 4) but is much more powerful in other respects, e. g. when drawing multiple curves. In general, it greatly improves graphics quality in most circumstances and otherwise leaves graphics elements as they are. Currently, the following features are implemented:

- Both straight lines and curves (solid, dashed, dotted and squiggled) are drawn by generic PDF commands.
- `Xy-pic` automatically draws the symbols of which lines and curves are composed at the very beginning and end of a segment. It then distributes the inner symbols evenly across the segment. Since the arc length of a Bézier curve is normally not proportional to its parameter, this is a nontrivial task in the case of curves. The `xypdf` package handles this better than the original code. Compare the output in Figure 2.

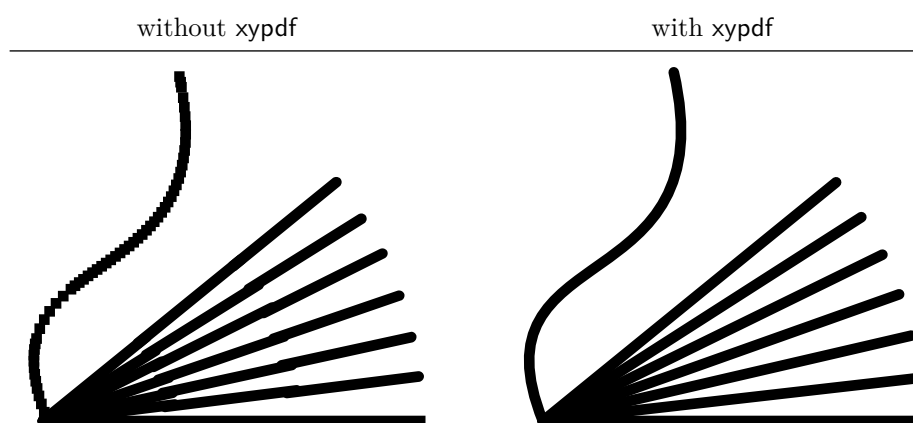
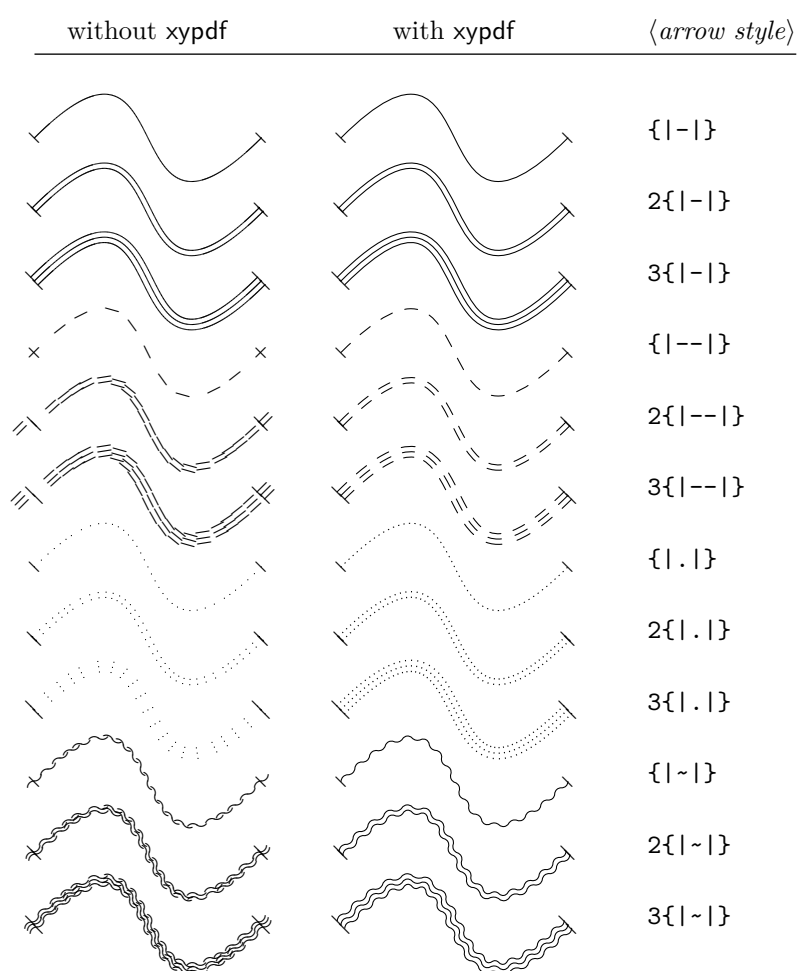


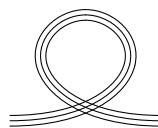
Figure 1: Comparison of Xy-pic output, magnified 10 times.




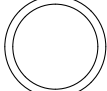
Code: `\xy (0,0) \ar @{\langle arrow\ style \rangle} ' {(20,20),(10,-20)} (30,0) \endxy`

Figure 2: Comparison of Xy-pic output for curves with various line styles.

- As a highlight, `xypdf` features a Bézier curve offset algorithm, producing high-quality curves with two or three parallel strokes.



- The `\cir` object draws circles of arbitrary radius.

without xypdf	with xypdf	code
		<code>\xy *\cir&lt;16pt&gt;{} *\cir&lt;19pt&gt;{} \endxy</code>

If you notice any unwanted behavior, please generate a minimal example and e-mail it to the author of this package. Current contact details are available at <http://www.math.uni-bonn.de/people/muellner>. Please report situations where the algorithms produce arithmetic overflows. Also, the code is not really optimized for speed but for accuracy, so feel free to report a significant slowdown of the compiling process for your thesis/paper/book.

## 2 Usage

Simply load the `xypdf` package after the `Xy-pic` package in your  $\text{\LaTeX}$  document.

```
\usepackage[<options>]{xy}
\usepackage{xypdf}
```

Do not use one of the driver options to `Xy-pic` like `dvips`, as the `xypdf` package does an analogous job to the Postscript drivers, and combining two drivers will usually result in mutilated diagrams.

The `xypdf` functionality can be switched off and on within the document by `\xypdfoff` and `\xypdfon`.

If  $\text{\LaTeX}$  complains ! No room for a new `\dimen`, try to load the `Xy-pic` and `xypdf` packages as early as possible. `xypdf` assigns 20 new dimension registers which are released at the end of the initialization. Thus, it needs 20 free dimension registers but will effectively not occupy new dimension registers.

## 3 Acknowledgements

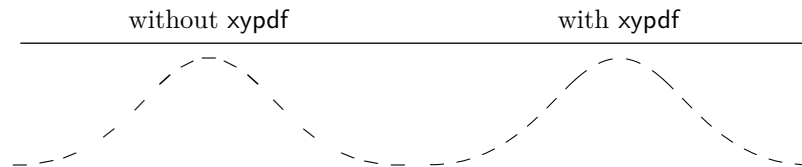
Since the `xypdf` package extends `Xy-pic`, some ideas are adopted from this package and its Postscript backend, and the author gratefully acknowledges the service which Kristoffer H. Rose and Ross Moore did to the mathematical community with their original package.

## 4 To do

- Code for the “line styles” extension.
- Code for scaling and rotating diagrams.

## 5 Caveat

Since the dashes in Bézier segments are aligned to the boundary points, this results in dashes of double length when a curve is composed of several Bézier segments. The original `Xy-pic` draws two dashes on top of each other at these positions.



code:

```
\xy (0,0);(50,0)
  **\crv{~**\dir{--} (10,0)&(20,15)&(30,15)&(40,0)}
\endxy
```

## 6 Copyright, license and disclaimer

The copyright for the xypdf package is by its author, Daniel Müllner. You may find current contact details at <http://www.math.uni-bonn.de/people/muellner>.

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## 7 Implementation

Test whether the Xy-pic package has been loaded properly.

```
1 \ifpackageloaded{xy}\relax
2   {\PackageError{xypdf}{Load the Xy-pic package before this package}
3     {Insert ‘\string\usepackage[<options>]{xy}’ before
4       ‘\string\usepackage{xypdf}’}}
5 \ifdefined\xypsloaded
6   \PackageError{xypdf}{Do not load Xy-pic with a Postscript backend}{}
7 \fi
```

Rely on the ifpdf package to test for PDF output.

```
8 \RequirePackage{ifpdf}
```

```
\xypdfon Commands for switching the extension on and off.
\xypdfoff
\xP@hook
9 \newcommand*\xypdfon{}
10 \newcommand*\xypdfoff{}
11 \newcommand*\xP@hook[1]{%
12   \edef\next@{%
13     \let\expandafter\noexpand\csname xP@old@#1\endcsname
14     \expandafter\noexpand\csname#1\endcsname}%
15   \next@
16   \edef\xypdfon{%
17     \unexpanded\expandafter{\xypdfon}%
18     \let\expandafter\noexpand\csname#1\endcsname
19     \expandafter\noexpand\csname xP@#1\endcsname
20   }%
21   \edef\xypdfoff{%
22     \unexpanded\expandafter{\xypdfoff}%
23     \let\expandafter\noexpand\csname#1\endcsname
24     \expandafter\noexpand\csname xP@old@#1\endcsname
25   }%
26 }
27 \AtEndOfPackage{\xypdfon\let\xP@hook\@undefined\let\xP@tempvar\@undefined}
```

`\xP@literal` Two possibilities to insert literal PDF commands, one for pdftex and one for dvipdfm(x)

```

28 \@ifdefinable\xP@literal\relax
29 \ifpdf
30 \let\xP@literal\pdfliteral
31 \else
32 \def\xP@literal#1{\special{pdf:literal #1}}
33 \fi

```

`\xP@dim` Conversion between T<sub>E</sub>X points (pt) and PDF/Postscript points (bp)

```

34 \newcommand*\xP@dim[1]{%
35 \expandafter\removePT@\the\dimexpr(#1)*800/803\relax\space}

```

`\xP@coord` Coordinates: two dimensions

```

36 \newcommand*\xP@coord[1]{\xP@dim{#1}\xP@dim}

```

`\xP@lw` Find out the default line width in the math fonts. This is done at the beginning of the document, when hopefully all potential changes to math fonts have taken place.

```

37 \AtBeginDocument{%
Initialize math fonts
38 {\setbox0\hbox{$ $}}%
39 \@ifdefinable\xP@lw\relax
40 \edef\xP@lw{\xP@dim{\fontdimen8\textfont3}}%
41 \PackageInfo{xypdf}{Line width: \the\fontdimen8\textfont3 }%
42 }

```

## 7.1 Straight lines

`\solid@` This is the hook for solid straight lines. Derived from `\xyPSSolid@` in `xyps.tex`.

`\xP@solid@`

```

43 \xP@hook{solid@}
44 \newcommand*\xP@solid@{\straight@\xP@solidSpread}

```

`\xP@solidSpread`

```

45 \@ifdefinable\xP@solidSpread\relax
46 \def\xP@solidSpread#1\repeat@{ {%
Neglect zero-length lines.
47 \@tempwatrue
48 \ifdim\X@p=\X@c
49 \ifdim\Y@p=\Y@c
50 \@tempwafalse
51 \fi
52 \fi
53 \if@tempwa
54 \xP@setsolidpat
55 \xP@stroke{\xP@coord\X@p\Y@p m \xP@coord\X@c\Y@c l}%
56 \fi
57 }}

```

`\xP@pattern`

```

58 \newcommand*\xP@pattern{}

```

`\xP@setsolidpat` Pattern for solid lines

```

59 \newcommand*\xP@setsolidpat{\def\xP@pattern{1 J 1 j []0 d }}

```

`\xP@stroke`

```

60 \newcommand*\xP@stroke[1]{\xP@literal{q \xP@lw w \xP@pattern#1 S Q}}

```

`\dash@` This is the hook for dashed straight lines. Derived from `\xyPSDashed@` in `xyps.tex`.

`\xP@dash@`

```

61 \xP@hook{dash@}
62 \newcommand\xP@dash@{\line@\def\Connect@@{\straight@\xP@dashedSpread}}

```

`\xP@dashedSpread`

```
63 \ifdefinable\xP@dashedSpread\relax
64 \def\xP@dashedSpread#1\repeat@{ {%
65   \xP@vecLen
```

Neglect zero-length lines.

```
66   \ifdim\@tempdimb>\z@
67     \xP@setdashpat
68     \xP@stroke{\xP@coord\X@p\Y@p m \xP@coord\X@c\Y@c l}%
69   \fi
70 }}
```

`\xP@setdashpat` The formula for the dash length is the same as in the `dashed` operator in `xypsdicte.tex`:

$$(\text{dash length}) = \frac{l}{2 \cdot \text{round}\left(\frac{l+d}{2d}\right) - 1},$$

where  $l$  is the length of the line and  $d$  is the minimal dash length.

The length  $l$  must be in `\@tempdimb`.

```
71 \newcommand*\xP@setdashpat{%
72   \edef\xP@pattern{1 J 1 j [%
73     \ifdim\@tempdimb>\xydashl@
74       \xP@dim{\@tempdimb/(2*\numexpr(\@tempdimb+\xydashl@))%
75         /(2*\xydashl@)\relax-1)}}%
76   \fi
77   ]0 d }}
```

`\point@` This is the hook for points. Derived from `\xyPSPoint@` in `xyps.tex`.

```
\xP@point@ 78 \xP@hook{point@}
79 \newcommand*\xP@point@{\xP@zerodot\egroup\Invisible@false
80   \Hidden@false\def\Leftness@{.5}\def\Upness@{.5}\ctipEdge@
81   \def\Drop@{\stylenboxz}%
82   \def\Connect@{\straight@\xP@dottedSpread}%
83 }
```

`\xP@zerodotpattern`

```
84 \newcommand*\xP@zerodotpattern{\def\xP@pattern{2 J [0 2]0 d }}
```

`\xP@zerodot`

```
85 \newcommand*\xP@zerodot{%
86   \xP@zerodotpattern
87   \xP@stroke{0 0 m 1 0 l}}
```

`\xP@dottedSpread`

```
88 \ifdefinable\xP@dottedSpread\relax
89 \def\xP@dottedSpread#1\repeat@{ {%
90   \xP@vecLen
91   \ifdim\@tempdimb>\z@
92     \xP@setdottedpat
93     \xP@stroke{\xP@coord\X@p\Y@p m \xP@coord\X@c\Y@c l}%
94   \fi
95 }}
```

`\xP@setdottedpat` The formula for the distance between dots is the same as in the `dotted` operator in `xypsdicte.tex`:

$$(\text{dot distance}) = \frac{l}{\text{round}\left(\frac{l}{2\text{pt}}\right) + 1},$$

where  $l$  is the length of the line.

The length  $l$  must be in `\@tempdimb`.

```
96 \newcommand*\xP@setdottedpat{\edef\xP@pattern{%
97   2 J [%
```

Produce a dot pattern only when the segment length is greater than the line width.

```

98 \ifdim\@tempdimb>\xP@lw bp
99 0 \xP@dim{\@tempdimb/\numexpr\@tempdimb/131072+1\relax}%
100 \fi
101 ]0 d
102 }}
```

In contrast to the Postscript drivers for  $\text{\texttt{Xy-pic}}$ , where some computations are left to the Postscript code, all arithmetic for the PDF output must be done by  $\text{\texttt{TeX}}$  itself. With  $\text{\texttt{TeX}}$ 's rudimentary fixed-point arithmetic, it is still a pain to compute even the length of a line segment, but things have become considerably easier with  $\varepsilon\text{\texttt{-TeX}}$ .

$\text{\texttt{\xP@abs}}$  Absolute value

```
103 \newcommand*\xP@abs[1]{\ifdim#1<z@\multiply#1@m@ne\fi}
```

$\text{\texttt{\xP@ifabsless}}$

```

104 \ifx\ifpdfabsdim\@undefined
105 \newcommand*\xP@ifabsless[2]{\ifdim\ifdim#1<z@-\fi#1<\ifdim#2<z@-\fi#2}
106 \gobble\fi
107 \else
108 \newcommand*\xP@ifabsless[2]{\ifpdfabsdim#1<#2}
109 \gobble\fi
110 \fi
```

$\text{\texttt{\xP@ifabsless@}}$

```

111 \newcommand*\xP@ifabsless@[4]{%
112 \xP@ifabsless{\dimexpr#1\relax}{\dimexpr#2\relax}#3\else#4\fi}
```

$\text{\texttt{\xP@swapdim}}$  Works unless parameter #2 is  $\text{\texttt{\@tempdima}}$ .

```
113 \newcommand*\xP@swapdim[2]{\@tempdima#1#2#2\@tempdima}
```

$\text{\texttt{\xP@swapnum}}$  Works unless parameter #2 is  $\text{\texttt{\@tempcnta}}$ .

```
114 \newcommand*\xP@swapnum[2]{\@tempcnta#1#2#2\@tempcnta}
```

$\text{\texttt{\xP@max}}$  Maximum of two lengths

```
115 \newcommand*\xP@max[2]{\ifdim#1>#2#1\else#2\fi}
```

$\text{\texttt{\xP@Max}}$  Assigns #1 the maximum of #1 and the absolute value of #2.

```
116 \newcommand*\xP@Max[2]{#1\ifdim#2<z@\xP@max#1{-#2}\else\xP@max#1#2\fi}
```

$\text{\texttt{\xP@sqrt}}$  Square root algorithm. The argument is in  $\text{\texttt{\@tempdima}}$ , and the start value for the iteration in  $\text{\texttt{\@tempdimc}}$ . The result goes into  $\text{\texttt{\@tempdimb}}$ .

```

117 \newcommand*\xP@sqrt{%
118 \loop
119 \@tempdimb\dimexpr(\@tempdimc+(\@tempdima*\p@/\@tempdimc))/2\relax
120 \ifdim\@tempdimc=\@tempdimb\else
iterate: (old approx.) := (new approx.)
121 \@tempdimc\@tempdimb\relax
122 \repeat
123 }
```

$\text{\texttt{\xP@veclen}}$  Absolute length of the vector  $(\text{\texttt{\d@X}}, \text{\texttt{\d@Y}})$ . The result goes into the register  $\text{\texttt{\@tempdimb}}$ . Several  $\text{\texttt{L\texttt{A}T\texttt{E}X}}$  registers are used as temporary registers, so this function is called safely within a group.

(Maybe it is not necessary to scale the coordinates so much as it is done here, and a simpler code would be fine as well.)

```

124 \newcommand*\xP@veclen{%
125 \xP@veclen@
126 \global\dimen@i\@tempdimb
```

```

127 }%
128 \@tempdimb\dimen@i
129 }

\XP@veclen@

130 \newcommand*\XP@veclen@{%
131   \XP@abs@d@Y
1) Strictly vertical vector
132   \ifdim\d@X=\z@
133     \@tempdimb@d@Y
134   \else
135     \XP@abs@d@X
2) Strictly horizontal vector
136   \ifdim\d@Y=\z@
137     \@tempdimb@d@X
138   \else
3) Diagonal vector.  $5931642\text{sp} = \sqrt{\text{maxdimen}/2}$ . Test whether the components are small
enough so that their sum of squares does not generate an arithmetic overflow.
139   \@tempswatrue
140   \ifdim\d@X>5931641sp\relax\@tempswafalse\fi
141   \ifdim\d@Y>5931641sp\relax\@tempswafalse\fi
142   \if@tempswa
3a) Small vector. \count@ contains a scaling factor for a precise fixed-point arithmetic.
143   \count@\@ne
144   \loop
145     \@tempdima\dimexpr\d@X*\d@X/\p@+\d@Y*\d@Y/\p@\relax
If the coordinates are small enough, scale them up to improve precision.
146   \ifdim\@tempdima<4096pt
147     \@tempcnta\ifdim\@tempdima<1024pt\ifdim\@tempdima<256pt8\else4\fi%
148     \else\tw@\fi
149     \multiply\d@X\@tempcnta
150     \multiply\d@Y\@tempcnta
151     \multiply\count@\@tempcnta
152   \repeat
Starting value for the square root algorithm
153   \@tempdimc\dimexpr(\d@X+\d@Y)*3/4\relax
154   \XP@sqr

Rescale
155   \@tempdimb\dimexpr\@tempdimb/\count@\relax
156   \else
157     \ifdim\d@X>83042982sp\relax\@tempswatrue\fi
158     \ifdim\d@Y>83042982sp\relax\@tempswatrue\fi
159     \if@tempswa
3b) Large vector. Scale the coordinates down to avoid an overflow.  $11927552\text{sp} = 182\text{pt}$ 
160     \@tempdima\dimexpr\d@X/182*\d@X/11927552+\d@Y/182*\d@Y/11927552\relax
161     \@tempdimc\dimexpr(\d@X+\d@Y)*3/728\relax
162     \XP@sqr
163     \multiply\@tempdimb182\relax
164     \else
3c) Medium vector. Also scale the coordinates down.  $12845056\text{sp} = 196\text{pt} = 14^2\text{pt}$ 
165     \@tempdima\dimexpr\d@X*\d@X/12845056+\d@Y*\d@Y/12845056\relax
166     \@tempdimc\dimexpr(\d@X+\d@Y)*3/56\relax
167     \XP@sqr
168     \multiply\@tempdimb14\relax
169     \fi

```



```

170      \fi
171      \fi
172  \fi
173 }

```

## 7.2 Squiggled lines

```

\squiggledSpread@ This is the hook for squiggled straight lines.
\xP@squiggledSpread@
174 \xP@hook{squiggledSpread@}
175 \@ifdefinable\xP@squiggledSpread@\relax
176 \def\xP@squiggledSpread@#1\repeat@{ {%
177   \xP@vecLen

```

Neglect zero-length lines.

```

178   \ifdim\@tempdimb>\z@
179     \edef\@tempa{\xP@coord\X@p\Y@p m }%
180     \toks@\expandafter{\@tempa}%

```

\@tempcnta = number of squiggles

```

181   \@tempcnta\numexpr\@tempdimb/\xybsqlll\relax
182   \ifnum\@tempcnta<\tw@\@tempcnta\tw@\fi
183   \@tempdima\dimexpr\d@X/\@tempcnta\relax
184   \@tempdimc\dimexpr\d@Y/\@tempcnta\relax
185   \count@\z@
186   \loop

```

The fraction is the continuous fraction approximation for the best spline approximation to a quarter circle ( $147546029/534618434 \approx \frac{1}{2} \cdot 0.55196760761152504532$ ).

```

187   \xP@append\toks@{%
188     \xP@coord{\X@p+\d@X*\count@/\@tempcnta+(\@tempdima
189       -\ifodd\count@-\fi\@tempdimc)*147546029/534618434}%
190     {\Y@p+\d@Y*\count@/\@tempcnta+(\@tempdimc
191       +\ifodd\count@-\fi\@tempdima)*147546029/534618434}%
192   }%
193   \advance\count@\@ne
194   \xP@append\toks@{%
195     \xP@coord{\X@p+\d@X*\count@/\@tempcnta-(\@tempdima
196       -\ifodd\count@-\fi\@tempdimc)*147546029/534618434}%
197     {\Y@p+\d@Y*\count@/\@tempcnta-(\@tempdimc
198       +\ifodd\count@-\fi\@tempdima)*147546029/534618434}%
199     \xP@coord{\X@p+\d@X*\count@/\@tempcnta}%
200     {\Y@p+\d@Y*\count@/\@tempcnta}%
201     c }%
202   \ifnum\count@<\@tempcnta
203     \repeat
204     \xP@setsolidpat
205     \xP@stroke{the\toks@}%
206   \fi
207 }

```

\xP@append

```

208 \newcommand*\xP@append[2]{ {%
209   \edef\@tempa{#1{the#1#2}}%
210   \expandafter}\@tempa
211 }

```

## 7.3 Temporary registers

In order to save registers, xypdf shares Xy-pic's dimension and counter registers but uses different, more descriptive names. Every macro that uses these temporary variables must

be safely encapsulated in a group so that the registers are not changed from the outside scope!

The xypdf package uses several sets of temporary variable names for different modules. Since it is important that these assignments do not overlap and that the variables are only used encapsulated within groups, the macros which use temporary variables are marked by colored bullets ●1, ●2, ●3, ●4, ●5, ●6, ●7 with one color for each set of variables.

The table in Figure 3 lists all variable assignments in these sets. It can be seen from the table which sets of variables can be used together. For example, set ●1 consisting of \xP@bigdim can be used together with all other temporary variables, while ●2 and ●4 must never be used together.

\xP@tempvar	
	212 \newcommand*\xP@tempvar[2]{%
	213 \ifdefinable#1\relax
	214 \let#1#2%
	215 }
\xP@bigdim	●1 A big constant less than $\frac{1}{3}\text{\maxdimen} \approx 5461\text{pt}$ and having many small prime factors.
	216 \xP@tempvar\xP@bigdim\quotPTK@
\xP@parA	●2 Second set of temporary variables: for the arc length algorithm.
\xP@velA	217 \xP@tempvar\xP@parA\L@p
\xP@parB	218 \xP@tempvar\xP@velA\U@p
\xP@velB	219 \xP@tempvar\xP@parB\R@p
\xP@parC	220 \xP@tempvar\xP@velB\D@p
\xP@velC	221 \xP@tempvar\xP@parC\X@origin
\xP@parD	222 \xP@tempvar\xP@velC\Y@origin
\xP@velD	223 \xP@tempvar\xP@parD\X@xbase
\xP@parE	224 \xP@tempvar\xP@velD\Y@xbase
\xP@velE	225 \xP@tempvar\xP@parE\X@ybase
\xP@lenA	226 \xP@tempvar\xP@velE\Y@ybase
\xP@lenB	227 \xP@tempvar\xP@lenA\X@min
\xP@partlen	228 \xP@tempvar\xP@lenB\Y@min
\xP@oldpartlen	229 \xP@tempvar\xP@partlen\X@max
\xP@tolerance	230 \xP@tempvar\xP@oldpartlen\Y@max
	231 \xP@tempvar\xP@tolerance\almostz@
\xP@A	●3 Third set of temporary registers: Bézier offset algorithm and solving linear equations.
\xP@B	232 \xP@tempvar\xP@A\L@p
\xP@C	233 \xP@tempvar\xP@B\U@p
\xP@D	234 \xP@tempvar\xP@C\R@p
\xP@E	235 \xP@tempvar\xP@D\D@p
\xP@F	236 \xP@tempvar\xP@E\X@origin
\xP@G	237 \xP@tempvar\xP@F\Y@origin
\xP@H	238 \xP@tempvar\xP@G\X@xbase
\xP@I	239 \xP@tempvar\xP@H\Y@xbase
\xP@J	240 \xP@tempvar\xP@I\X@ybase
\xP@K	241 \xP@tempvar\xP@J\Y@ybase
\xP@L	242 \xP@tempvar\xP@K\X@min
\xP@fa	243 \xP@tempvar\xP@L\Y@min
\xP@fd	244 \xP@tempvar\xP@fa\X@max
\xP@tm	245 \xP@tempvar\xP@fd\Y@max
\xP@xm	246 \xP@tempvar\xP@tm\almostz@
\xP@ym	247 \xP@tempvar\xP@xm\K@dXdY
	248 \xP@tempvar\xP@ym\K@dYdX

●3 Alas, we need 20 more temporary registers. Hopefully, there are still free slots for dimension registers. We take them for the temporary variables but release them afterwards so that other packages can use them.

Xy-pic var.	Set 1	Set 2	Set 3	Set 4	Set 5	Set 6	Set 7
\quotPTK@	\xP@bigdim						
\L@p	\xP@parA		\xP@A		(\L@p)		(\L@p)
\U@p	\xP@velA		\xP@B		(\U@p)		(\U@p)
\R@p	\xP@parB		\xP@C		(\R@p)		(\R@p)
\D@p	\xP@velB		\xP@D		(\D@p)		(\D@p)
\X@origin	\xP@parC		\xP@E				\xP@temppar
\Y@origin	\xP@velC		\xP@F				\xP@tempvel
\X@xbase	\xP@parD		\xP@G				\xP@posX
\Y@xbase	\xP@velD		\xP@H				\xP@posY
\X@ybase	\xP@parE		\xP@I		\xP@a		\xP@oldpar
\Y@ybase	\xP@velE		\xP@J		\xP@b		\xP@lastpar
\X@min	\xP@lenA		\xP@K		\xP@c		\xP@tempvel@
\Y@min	\xP@lenB		\xP@L		\xP@valA		
\X@max	\xP@partlen		\xP@fa		\xP@valB		
\Y@max	\xP@oldpartlen		\xP@fd		\xP@devA		
\almostz@	\xP@tolerance		\xP@tm		\xP@devB		
\K@dXdY			\xP@xm		\xP@ti		
\K@dYdX			\xP@ym		\xP@tip		
new var. 1			\xP@off		(\xP@off)		
new var. 2			\xP@ta				
new var. 3			\xP@tb				
new var. 4			\xP@tc				
new var. 5			\xP@M				
new var. 6			\xP@oldobj				
new var. 7			\xP@Tax			\xP@sa	
new var. 8			\xP@Tay			\xP@sb	
new var. 9			\xP@Tdx			\xP@sc	
new var. 10			\xP@Tdy			\xP@Ab	
new var. 11			\xP@Tmx			\xP@AAb	
new var. 12			\xP@Tmy			\xP@Aba	
new var. 13			\xP@xa	(\xP@xa)		\xP@Abb	
new var. 14			\xP@ya	(\xP@ya)		\xP@Abc	
new var. 15			\xP@xb	(\xP@xb)		\xP@AAba	
new var. 16			\xP@yb	(\xP@yb)		\xP@AAbb	
new var. 17			\xP@xc	(\xP@xc)		\xP@AAbc	
new var. 18			\xP@yc	(\xP@yc)		\xP@dta	
new var. 19			\xP@xd	(\xP@xd)		\xP@dtb	
new var. 20			\xP@yd	(\xP@yd)		\xP@dtc	

Figure 3: Temporary dimension registers in xypdf.

`\xP@off`    ●3  
`\xP@ta`    249 `\@tempcnta\count11\relax`  
`\xP@tb`    250 `\newdimen\xP@off`  
`\xP@tc`    251 `\newdimen\xP@ta`  
`\xP@M`    252 `\newdimen\xP@tb`  
`\xP@oldobj` 253 `\newdimen\xP@tc`  
`\xP@Tax`    254 `\newdimen\xP@M`  
`\xP@Tay`    255 `\newdimen\xP@oldobj`  
`\xP@Tdx`    256 `\newdimen\xP@Tax`  
`\xP@Tdy`    257 `\newdimen\xP@Tay`  
`\xP@Tdx`    258 `\newdimen\xP@Tdx`  
`\xP@Tmx`    259 `\newdimen\xP@Tdy`  
`\xP@Tmy`    260 `\newdimen\xP@Tmx`  
`\xP@xa`    261 `\newdimen\xP@Tmy`  
`\xP@ya`    262 `\newdimen\xP@xa`  
`\xP@xb`    263 `\newdimen\xP@ya`  
`\xP@yb`    264 `\newdimen\xP@xb`  
`\xP@xc`    265 `\newdimen\xP@yb`  
`\xP@yc`    266 `\newdimen\xP@xc`  
`\xP@xd`    267 `\newdimen\xP@yc`  
`\xP@yd`    268 `\newdimen\xP@xd`  
`\xP@yd`    269 `\newdimen\xP@yd`  
`\xP@yd`    270 `\count11\@tempcnta`

`\xP@a`    ●5 Fifth set of temporary variables: Parameters for drawing part of a spline segment.  
`\xP@b`    271 `\xP@tempvar\xP@a\X@ybase`  
`\xP@c`    272 `\xP@tempvar\xP@b\Y@ybase`  
`\xP@valA` 273 `\xP@tempvar\xP@c\X@min`  
`\xP@valB` 274 `\xP@tempvar\xP@valA\Y@min`  
`\xP@devA` 275 `\xP@tempvar\xP@valB\X@max`  
`\xP@devB` 276 `\xP@tempvar\xP@devA\Y@max`  
`\xP@ti`    277 `\xP@tempvar\xP@devB\almostz@`  
`\xP@tip`    278 `\xP@tempvar\xP@ti\K@dXdY`  
`\xP@tip`    279 `\xP@tempvar\xP@tip\K@dYdX`

`\xP@sa`    ●6 Sixth set of temporary variables: Solving a linear system approximately.  
`\xP@sb`    280 `\xP@tempvar\xP@sa\xP@Tax`  
`\xP@sc`    281 `\xP@tempvar\xP@sb\xP@Tay`  
`\xP@Ab`    282 `\xP@tempvar\xP@sc\xP@Tdx`  
`\xP@AAb`    283 `\xP@tempvar\xP@Ab\xP@Tdy`  
`\xP@Aba`    284 `\xP@tempvar\xP@AAb\xP@Tmx`  
`\xP@Abb`    285 `\xP@tempvar\xP@Aba\xP@Tmy`  
`\xP@Abc`    286 `\xP@tempvar\xP@Abb\xP@xa`  
`\xP@AAba`    287 `\xP@tempvar\xP@Abc\xP@ya`  
`\xP@AAbb`    288 `\xP@tempvar\xP@AAba\xP@xb`  
`\xP@AAbc`    289 `\xP@tempvar\xP@AAbb\xP@yb`  
`\xP@AAbc`    290 `\xP@tempvar\xP@AAbc\xP@xc`  
`\xP@dta`    291 `\xP@tempvar\xP@dta\xP@yc`  
`\xP@dtb`    292 `\xP@tempvar\xP@dtb\xP@xd`  
`\xP@dtc`    293 `\xP@tempvar\xP@dtc\xP@yd`

`\xP@temppar` ●7 Seventh set of temporary registers: For multiple dotted splines.  
`\xP@tempvel` 294 `\xP@tempvar\xP@temppar\X@origin`  
`\xP@posX`    295 `\xP@tempvar\xP@tempvel\Y@origin`  
`\xP@posY`    296 `\xP@tempvar\xP@posX\X@xbase`  
`\xP@oldpar`    297 `\xP@tempvar\xP@posY\Y@xbase`  
`\xP@lastpar` 298 `\xP@tempvar\xP@oldpar\X@ybase`  
`\xP@tempvel@` 299 `\xP@tempvar\xP@lastpar\Y@ybase`  
`\xP@tempvel@` 300 `\xP@tempvar\xP@tempvel@X@min`

`\xP@scaleone` We also use temporary numerical registers for scaling factors in `\xP@solvelinearsystem`.  
`\xP@scaletwo` 301 `\xP@tempvar\xP@scaleone\K@`  
`\xP@scalethree` 302 `\xP@tempvar\xP@scaletwo\KK@`  
303 `\xP@tempvar\xP@scalethree\Direction`

## 7.4 Bézier curves

`\splinesolid@` These are the hooks for splines (solid, dashed and dotted).  
`\splinedashed@` 304 `\xP@hook{splinesolid@}`  
`\splinedotted@` 305 `\newcommand*\xP@splinesolid@{\xP@spline\xP@setsolidpat}`  
306 `\xP@hook{splinedashed@}`  
307 `\newcommand*\xP@splinedashed@{\xP@spline\xP@setdashpat}`  
308 `\xP@hook{splinedotted@}`  
309 `\newcommand*\xP@splinedotted@{\xP@spline\xP@setdottedpat}`

`\xP@spline` Output a spline segment. Parameter: Macro for the dash pattern generation.

310 `\newcommand*\xP@spline[1]{%`  
311 `\readsplineparams@`  
312 `\ifdim\dimen5<\dimen7`  
313 `\xP@preparespline`  
314 `\ifdim\@tempdimb>\z@`  
315 `#1%`  
316 `\xP@stroke{\xP@coord\X@p\Y@p m %`  
317 `\xP@coord\L@c\U@c\xP@coord\R@c\D@c\xP@coord\X@c\Y@c c}%`  
318 `\fi`  
319 `\fi`  
320 `}`

`\xP@preparespline`

321 `\newcommand*\xP@preparespline{%`  
If we have a quadratic Bézier segment, convert it to a cubic one.  
322 `\ifx\splineinfo@\squineinfo@`  
323 `\L@c\dimexpr(\X@p+2\A@)/3\relax`  
324 `\U@c\dimexpr(\Y@p+2\B@)/3\relax`  
325 `\R@c\dimexpr(\X@c+2\A@)/3\relax`  
326 `\D@c\dimexpr(\Y@c+2\B@)/3\relax`  
327 `\fi`  
328 `\xP@shavespline`  
329 `\xP@bezierlength`  
330 `}`

`\xP@inibigdim` •1 Initialize `\xP@bigdim` every time a macro that uses this register is called. See e.g. `\xP@shaveprec`.

331 `\newcommand*\xP@inibigdim{\xP@bigdim5040pt}`

`\xP@shavespline` Shave a cubic spline at both ends at the parameter values in `\dimen5` and `\dimen7`. For normal use, the parameters fulfill  $0\text{pt} \leq \dimen5 < \dimen7 \leq 1\text{pt}$ .

(Note that `\xP@bigdim` only occurs in the arguments to `\xP@shaveprec`, so this use is safe.)

332 `\newcommand*\xP@shavespline{%`  
333 `\xP@shaveprec{\dimen5*\xP@bigdim/\p@}{\dimen7*\xP@bigdim/\p@}%`  
334 `}`

`\xP@shaveprec` •1 Shave a cubic spline at both ends at the parameter values in #1 and #2. For normal use, the parameters fulfill  $0\text{pt} \leq \#1 < \#2 \leq \xP@bigdim$ . The control points for the cubic Bézier curve are  $(\X@p, \Y@p)$ ,  $(\L@c, \U@c)$ ,  $(\R@c, \D@c)$ ,  $(\X@c, \Y@c)$ . The  $\X$ -pic registers `\A@`, `\B@`, `\L@p`, `\U@p`, `\R@p`, `\D@p`, `\X@min` and `\Y@min` are used as temporary registers, but safely encapsulated in a group.

```

335 \newcommand*\xP@shaveprec[2]{\%
336   \xP@inibigdim
337   \A@\dimexpr#1\relax
338   \B@\dimexpr#2\relax
339   \@tempswatrue
340   \ifdim\A@=\z@\ifdim\B@=\xP@bigdim\@tempswafalse\fi\fi
341   \if@tempswa
342     \L@p\dimexpr\L@c-\X@p\relax
343     \U@p\dimexpr\R@c-\L@p-\L@c\relax
344     \R@p\dimexpr\X@c-3\R@c+3\L@c-\X@p\relax
345     \D@p\dimexpr\U@c-\Y@p\relax
346     \X@min\dimexpr\D@c-\D@p-\U@c\relax
347     \Y@min\dimexpr\Y@c-3\D@c+3\U@c-\Y@p\relax
348     \xdef\@gtempa{\%
349       \X@p\the\dimexpr\X@p+(3\L@p+(3\U@p+\R@p*\A@/\xP@bigdim)\%
350         *\A@/\xP@bigdim)*\A@/\xP@bigdim\relax
351       \Y@p\the\dimexpr\Y@p+(3\D@p+(3\X@min+\Y@min*\A@/\xP@bigdim)\%
352         *\A@/\xP@bigdim)*\A@/\xP@bigdim\relax
353       \L@c\the\dimexpr\X@p+(2\A@+\B@)*\L@p/\xP@bigdim+((\A@+2\B@)\%
354         *\U@p/\xP@bigdim+\R@p*\A@/\xP@bigdim*\B@/\xP@bigdim)\%
355         *\A@/\xP@bigdim\relax
356       \U@c\the\dimexpr\Y@p+(2\A@+\B@)*\D@p/\xP@bigdim+((\A@+2\B@)\%
357         *\X@min/\xP@bigdim+\Y@min*\A@/\xP@bigdim*\B@/\xP@bigdim)\%
358         *\A@/\xP@bigdim\relax
359       \R@c\the\dimexpr\X@p+(2\B@+\A@)*\L@p/\xP@bigdim+((\B@+2\A@)\%
360         *\U@p/\xP@bigdim+\R@p*\B@/\xP@bigdim*\A@/\xP@bigdim)\%
361         *\B@/\xP@bigdim\relax
362       \D@c\the\dimexpr\Y@p+(2\B@+\A@)*\D@p/\xP@bigdim+((\B@+2\A@)\%
363         *\X@min/\xP@bigdim+\Y@min*\B@/\xP@bigdim*\A@/\xP@bigdim)\%
364         *\B@/\xP@bigdim\relax
365       \X@c\the\dimexpr\X@p+(3\L@p+(3\U@p+\R@p*\B@/\xP@bigdim)\%
366         *\B@/\xP@bigdim)*\B@/\xP@bigdim\relax
367       \Y@c\the\dimexpr\Y@p+(3\D@p+(3\X@min+\Y@min*\B@/\xP@bigdim)\%
368         *\B@/\xP@bigdim)*\B@/\xP@bigdim\relax}%
369   \else
370     \global\let\@gtempa\relax
371   \fi
372 } \@gtempa
373 }

```

`\xP@bezierlength` •2 Compute the arc length of a cubic Bézier segment.

The following algorithm is used: The velocity for a partial segment is fitted at three points (A-C-E) by a quadratic function, and the arc length is approximated by the integral over this quadratic function.

Each interval is recursively divided in halves (A-B-C, C-D-E) as long as the result for the arc length changes more than the precision parameter `\xP@tolerance`. If the desired precision is reached, the arc length in the small interval is added to the total arc length, and the next interval is considered.

The result goes into `\@tempdimb`.

```

374 \newcommand*\xP@bezierlength{\%
375   \@tempdimb\z@
376   \xP@parA\z@
377   \xP@velocity\z@\xP@velA
378   \xP@parC.5\p@
379   \xP@velocity\xP@parC\xP@velC
380   \xP@velocity\p@\xP@velE

```

Arc length (integral over the quadratic approximation)

```

381   \xP@oldpartlen\dimexpr(\xP@velA+4\xP@velC+\xP@velE)/6\relax

```

Tolerance parameter: It is set to  $1/65536$  of the approximate arc length, but at least 1sp (e. g. for closed arcs).

```
382 \xP@tolerance\xP@max{1sp}{\dimexpr\xP@oldpartlen/\p@\relax}%
```

Initiate the recursive algorithm with the interval  $[0, 1]$ .

```
383 \xP@arclength\xP@parC\xP@velC\p@\xP@velE\xP@oldpartlen
```

Pass the result to outside the group.

```
384 \global\dimen@i\@tempdimb
385 }\@tempdimb\dimen@i
386 }
```

**\xP@velocity** •5 Compute the velocity at the point #1 on a cubic Bézier curve. Needs: Bézier control points  $\backslash X@p, \dots, \backslash Y@c$ . Parameter #2: dimension register for the result. Temporary:  $\backslash L@p, \backslash U@p, \backslash d@X, \backslash d@Y$ .

```
387 \newcommand*\xP@velocity[2]{%
388 \@tempdima\dimexpr#1\relax
389 \xP@velocity@
390 \global\dimen@i\@tempdimb
391 }#2\dimen@i
392 }
```

**\xP@velocity@** •5

```
393 \newcommand*\xP@velocity@{%
394 \L@p\dimexpr\L@c-\X@p\relax
395 \U@p\dimexpr\U@c-\Y@p\relax
396 \d@X3\dimexpr((\X@c+(\L@c-\R@c)*3-\X@p)*\@tempdima/\p@
397 +(\R@c-\L@p-\L@c)*2)*\@tempdima/\p@+\L@p\relax
398 \d@Y3\dimexpr((\Y@c+(\U@c-\D@c)*3-\Y@p)*\@tempdima/\p@
399 +(\D@c-\U@p-\U@c)*2)*\@tempdima/\p@+\U@p\relax
400 \xP@vecclen
401 }
```

**\xP@velocity@@** •5

```
402 \newcommand*\xP@velocity@@{%
403 \R@p\dimexpr\xP@xb-\xP@xa\relax
404 \D@p\dimexpr\xP@yb-\xP@ya\relax
405 \d@X3\dimexpr((\xP@xd+(\xP@xb-\xP@xc)*3-\xP@xa)*\@tempdima/\p@
406 +(\xP@xc-\R@p-\xP@xb)*2)*\@tempdima/\p@+\R@p\relax
407 \d@Y3\dimexpr((\xP@yd+(\xP@yb-\xP@yc)*3-\xP@ya)*\@tempdima/\p@
408 +(\xP@yc-\D@p-\xP@yb)*2)*\@tempdima/\p@+\D@p\relax
409 \xP@vecclen
410 }
```

**\xP@normalvec** •5 Normal vector on a Bézier curve. Parameter: Parameter on segment, normal distance. Needs: Bézier parameters  $\backslash X@p, \dots, \backslash Y@c$

```
411 \newcommand*\xP@normalvec[2]{%
412 \@tempdima#1\relax
413 \@tempdimc#2\relax
414 \xP@velocity@
```

If the velocity is zero at some point, take the third derivative for the tangent vector.

```
415 \ifdim\@tempdimb=\z@
416 \d@X\dimexpr\xP@xd+(\xP@xb-\xP@xc)*3-\xP@xa\relax
417 \d@Y\dimexpr\xP@yd+(\xP@yb-\xP@yc)*3-\xP@ya\relax
418 \xP@vecclen
419 \ifdim\@tempdimb=\z@
420 \PackageError{xypdf}{Cannot determine a tangent vector to a curve}{}%
421 \@tempdimb\p@
422 \fi
423 \fi
```

```

424 \global\dimen@i\dimexpr\@tempdimc*\d@Y/\@tempdimb\relax
425 \global\dimen3\dimexpr-\@tempdimc*\d@X/\@tempdimb\relax
426 }%
427 \d@X\dimen@i
428 \d@Y\dimen3\relax
429 }

```

\xP@arclength ●2 The recursive step for the arc length computation.

Needs: \xP@tolerance, \xP@parA, \xP@velA. Parameter: #1 is the middle parameter, #2 the velocity at #1, #3 the third parameter, #4 the velocity at #3, #5 the approximate arc length in the interval from \xP@parA to #3.

```

430 \newcommand*\xP@arclength[5]{%
431 \xP@parE#3%
432 \xP@velE#4%
433 \xP@parC#1%
434 \xP@velC#2%
435 \xP@oldpartlen#5%

```

Compute two more pairs (parameter, velocity) at positions  $\frac{1}{4}$  and  $\frac{3}{4}$  of the interval.

```

436 \xP@parB\dimexpr(\xP@parC+\xP@parA)/2\relax
437 \xP@velocity\xP@parB\xP@velB
438 \xP@parD\dimexpr(\xP@parE+\xP@parC)/2\relax
439 \xP@velocity\xP@parD\xP@velD

```

Compute the approximations for the arc length on the two smaller parameter intervals (A-B-C) and (C-D-E).

```

440 \xP@lenA
441 \dimexpr(\xP@velA+4\xP@velB+\xP@velC)*(\xP@parC-\xP@parA)/393216\relax
442 \xP@lenB
443 \dimexpr(\xP@velC+4\xP@velD+\xP@velE)*(\xP@parE-\xP@parC)/393216\relax
444 \xP@partlen\dimexpr\xP@lenA+\xP@lenB\relax

```

Check whether the approximation for the arc length has changed more than the precision parameter. The code is a hack to compare the absolute value without occupying another dimension register.

```

445 {\@tempdima\dimexpr\xP@oldpartlen-\xP@partlen\relax
446 \expandafter}\ifdim\ifdim\@tempdima<\z@-\fi\@tempdima>\xP@tolerance

```

Yes? Subdivide the interval. The input queue serves as a LIFO stack here!

```

447 \edef\next@{%
448 \noexpand\xP@arclength\xP@parB\xP@velB\xP@parC\xP@velC\xP@lenA
449 \noexpand\xP@arclength{\the\xP@parD}{\the\xP@velD}{\the\xP@parE}%
450 {\the\xP@velE}{\the\xP@lenB}%
451 }%
452 \else

```

No? Proceed to the next parameter interval.

```

453 \xP@parA\xP@parE
454 \xP@velA\xP@velE
455 \advance\@tempdimb\xP@partlen
456 \DN@{}%
457 \fi
458 \next@
459 }

```

## 7.5 New improved curve styles

\@crv@ Extend the list of curve styles for which special routines exist.

```

460 \CheckCommand*\@crv@[2]{\DN@{#1#2}%
461 \ifx\next@\empty \edef\next@{\crv@defaultshape}%
462 \ifx\bstartPLACE@\empty \xdef\crvSTYLE@{\crv@defaultshape}}\fi
463 \else

```



```

464 \ifx\bstartPLACE@empty\gdef\crvSTYLE@{#1{#2}}\fi
465 \fi
466 \ifx\next@empty\crv@noobject\DN@{\crv@}{\xy@crvaddstack@}%
467 \else\def\tmp@{-}\ifx\next@\tmp@\DN@{\crv@}{\xy@crvaddstack@}%
468 \else\def\tmp@={}\ifx\next@\tmp@
469 \DN@{\expandafter\crv@\crv@normaltemplate{\dir{=}}}%
470 \else\def\tmp@{2-}\ifx\next@\tmp@
471 \DN@{\expandafter\crv@\crv@normaltemplate{\dir{2.}}}%
472 \else\def\tmp@{3-}\ifx\next@\tmp@
473 \DN@{\expandafter\crv@\crv@normaltemplate{\dir{3.}}}%
474 \else\def\tmp@{--}\ifx\next@\tmp@
475 \DN@{\expandafter\crv@\crv@specialtemplate@{--}}%
476 \else\def\tmp@{==}\ifx\next@\tmp@
477 \DN@{\expandafter\crv@\crv@normaltemplate{\dir2{--}}}
478 \else\def\tmp@{2--}\ifx\next@\tmp@
479 \DN@{\expandafter\crv@\crv@normaltemplate{\dir2{--}}}
480 \else\def\tmp@{3--}\ifx\next@\tmp@
481 \DN@{\expandafter\crv@\crv@normaltemplate{\dir3{--}}}
482 \else\def\tmp@{.}\ifx\next@\tmp@
483 \DN@{\expandafter\crv@\crv@specialtemplate@{.}}%
484 \else\def\tmp@{:}\ifx\next@\tmp@
485 \DN@{\expandafter\crv@\crv@normaltemplate{\dir{:}}}%
486 \else\def\tmp@{2.}\ifx\next@\tmp@
487 \DN@{\expandafter\crv@\crv@normaltemplate{\dir{:}}}%
488 \else\def\tmp@{..}\ifx\next@\tmp@
489 \DN@{\expandafter\crv@\crv@specialtemplate@{.}}%
490 \else
491 \DN@{\expandafter\crv@\crv@othertemplate{\dir#1{#2}}}%
492 \fi\fi\fi\fi\fi\fi\fi\fi\fi\fi\fi\fi\fi\fi\next@}

```

493 \xP@hook{@crv@}

```

494 \newcommand*\xP@crv@[2]{\DN@{#1#2}%
495 \ifx\next@empty \edef\next@{\crv@defaultshape}%
496 \ifx\bstartPLACE@empty \xdef\crvSTYLE@{\crv@defaultshape}}\fi
497 \else
498 \ifx\bstartPLACE@empty \gdef\crvSTYLE@{#1#2}}\fi
499 \fi
500 \ifx\next@empty \crv@noobject \DN@{\crv@}{\xy@crvaddstack@}%
501 \else\def\tmp@{-}\ifx\next@tmp@ \DN@{\crv@}{\xy@crvaddstack@}%
502 \else\def\tmp@{=}\ifx\next@tmp@
503 \DN@{\expandafter\crv@\crv@normaltemplate{\dir{=}}}%
504 \else\def\tmp@{2-}\ifx\next@tmp@
505 \DN@{\expandafter\crv@\crv@normaltemplate{\dir{2.}}}%
506 \else\def\tmp@{3-}\ifx\next@tmp@
507 \DN@{\expandafter\crv@\crv@normaltemplate{\dir{3.}}}%
508 \else\def\tmp@{--}\ifx\next@tmp@
509 \DN@{\expandafter\crv@\crv@specialtemplate@{--}}%
510 \else\def\tmp@{==}\ifx\next@tmp@
511 \DN@{\expandafter\crv@\crv@normaltemplate{\dir2{--}}}%
512 \else\def\tmp@{2--}\ifx\next@tmp@
513 \DN@{\expandafter\crv@\crv@normaltemplate{\dir2{--}}}%
514 \else\def\tmp@{3--}\ifx\next@tmp@
515 \DN@{\expandafter\crv@\crv@normaltemplate{\dir3{--}}}%
516 \else\def\tmp@{.}\ifx\next@tmp@
517 \DN@{\expandafter\crv@\crv@specialtemplate@{.}}%
518 \else\def\tmp@{:}\ifx\next@tmp@
519 \DN@{\expandafter\crv@\crv@normaltemplate{\dir{:}}}%
520 \else\def\tmp@{2.}\ifx\next@tmp@

```



## 7.6 Multiple solid curves

```

\XP@splinedoubled@
576 \XP@hook{splinedoubled@}
577 \newcommand*\XP@splinedoubled@{%
578   \XP@checkspline\XP@splinemultsolid\XP@doublestroke}

\XP@splineribboned@
579 \XP@hook{splineribboned@}
580 \@ifdefinable\XP@splineribboned@\relax
581 \let\XP@splineribboned@\XP@splinedoubled@

\XP@splinetrebled@
582 \XP@hook{splinetrebled@}
583 \newcommand*\XP@splinetrebled@{%
584   \XP@checkspline\XP@splinemultsolid\XP@trblstroke}

\XP@doublestroke Offset parameters for double lines and curves
585 \newcommand*\XP@doublestroke{\xydashh@/2,-\xydashh@/2}

\XP@trblstroke Offset parameters for treble lines and curves
586 \newcommand*\XP@trblstroke{\xydashh@,\z@,-\xydashh@}

\XP@checkspline Get and check spline parameters before the macro in #1 is executed.
587 \newcommand*\XP@checkspline[1]{%
588   \readsplineparams@
Neglect splines which are drawn “backwards”. Somehow Xy-pic draws curves forward and
backward, but we need it to be drawn only once.
589   \let\next@\@gobble
590   \ifdim\dimen5<\dimen7
591     \XP@preparespline
Neglect splines of zero length.
592     \ifdim\@tempdimb>\z@
If the path length is less than the line width, just draw a solid path.
593       \ifdim\@tempdimb<\XP@lw bp
594         \let\next@\XP@splinemultsolid
595       \else
596         \let\next@#1%
597       \fi
598     \fi
599   \fi
600   \next@
601 }

\XP@splinemultsolid •1
602 \newcommand*\XP@splinemultsolid[1]{%
603   \XP@inibigdim
604   \@temptokena{}%
605   \XP@setsolidpat
606   \@for\@tempa:=#1\do{\XP@paintsolid\z@\XP@bigdim}%
607   \XP@stroke{\the\@temptokena}%
608 }}

\XP@paintsolid •1 •5
609 \newcommand*\XP@paintsolid[2]{%

```

Record the original anchor points.

```

610 \xP@savepts
611 \xP@a#1\relax
612 \xP@c#2\relax
613 \xP@movetotruer
614 \xP@paintsolid@
615 \xdef\@gtempa{\the\@temptokena}%
616 }%
617 \@temptokena\expandafter{\@gtempa}%
618 }

```

\xP@paintsolid@ ●1 ●5

```

619 \newcommand*\xP@paintsolid@{%

```

These parameters record which part of the spline is currently being offset. They are varied as the spline may be subdivided for a precise offset curve.

```

620 \xP@b\xP@c

```

Offset distance

```

621 \xP@off\dimexpr\@tempa\relax
622 \ifdim\xP@off=\z@
623 \xP@shaveprec\xP@a\xP@c
624 \else
625 \loop

```

Restore the original anchor points.

```

626 \xP@restorepts

```

Cut out the current portion of the spline.

```

627 \xP@shaveprec\xP@a\xP@b

```

Compute the approximate offset curve.

```

628 \xP@offsetsegment

```

Test if the offset curve is good enough.

```

629 \xP@testoffset

```

If not, shorten the parameter interval by 30%.

```

630 \ifxP@offsetok
631 \else
632 \xP@b\dimexpr\xP@a+(\xP@b-\xP@a)*7/10\relax
633 \repeat
634 \fi

```

Append the new segment to the path.

```

635 \xP@append\@temptokena{\ifxP@moveto\xP@coord\X@p\Y@p m \fi
636 \xP@coord\l@c\U@c\xP@coord\R@c\D@c\xP@coord\X@c\Y@c c }%
637 \xP@movetofalse

```

Test if the end of the spline has been reached. If not, offset the rest of the curve.

```

638 \ifdim\xP@b<\xP@c\relax
639 \xP@a\xP@b
640 \expandafter\xP@paintsolid@
641 \fi
642 }

```

\ifxP@moveto We need a PDF moveto operator only for the first partial segment. Additional segments connect seamlessly.

```

643 \newif\ifxP@moveto

```

\xP@savepts ●5 Save the anchor points to the second set of reserved variables.

```

644 \newcommand*\xP@savepts{%
645 \xP@xa\X@p
646 \xP@ya\Y@p

```

```

647 \xP@xb\L@c
648 \xP@yb\U@c
649 \xP@xc\R@c
650 \xP@yc\D@c
651 \xP@xd\X@c
652 \xP@yd\Y@c
653 }

```

\xP@restorepts •5 Restore the anchor points from the second set of reserved variables.

```

654 \newcommand*\xP@restorepts{%
655 \X@p\xP@xa
656 \Y@p\xP@ya
657 \L@c\xP@xb
658 \U@c\xP@yb
659 \R@c\xP@xc
660 \D@c\xP@yc
661 \X@c\xP@xd
662 \Y@c\xP@yd
663 }

```

## 7.7 A Bézier curve offset algorithm

First, all control points are offset by the desired distance and in the direction of the normal vectors at the boundary points of the curve. We then adjust the distance of the inner two control points to the boundary control points along the tangents at the boundary points:  $x_b = x_a + f_a T_{ax}$ ,  $x_c = x_d + f_d T_{dx}$ , and likewise for the  $y$ -coordinates. In nondegenerate cases, we have  $T_{ax} = x_b - x_a$  and  $T_{dx} = x_c - x_d$ .

Let  $P(a, b, c, d, t)$  denote the Bézier polynomial  $a(1-t)^3 + 3bt(1-t)^2 + 3ct^2(1-t) + dt^3$ . In order to determine the factors  $f_a$  and  $f_d$ , we set up a system of three equations.

- Two equations: The old point at parameter  $\frac{1}{2}$  plus offset,  $(x_m, y_m)$ , is the new point at parameter  $t_m$ .

$$\begin{aligned}
 x_m &= P(x_a, x_a + f_a T_{ax}, x_d + f_d T_{dx}, x_d, t_m) \\
 y_m &= P(y_a, y_a + f_a T_{ay}, y_d + f_d T_{dy}, y_d, t_m)
 \end{aligned}$$

- Third equation: The old tangent at parameter  $\frac{1}{2}$  is in the same direction as the new tangent at  $t_m$ .

$$\begin{aligned}
 &\frac{\partial}{\partial t_m} P(x_a, x_a + f_a T_{ax}, x_d + f_d T_{dx}, x_d, t_m) \cdot T_{my} \\
 &= \frac{\partial}{\partial t_m} P(y_a, y_a + f_a T_{ay}, y_d + f_d T_{dy}, y_d, t_m) \cdot T_{mx}
 \end{aligned}$$

Up to a scalar factor of  $-3/4$ ,  $(T_{mx}, T_{my})$  is the velocity vector to the original curve at parameter  $\frac{1}{2}$ . We have  $T_{mx} = (X_a + X_b - X_c - X_d)/2$  (in the old coordinates!) and  $T_{my}$  analogously. The system above is a nonlinear system of three equations in three variables, which we solve by Newton's method. Let  $f_a$ ,  $f_d$ , and  $t_m$  be approximate solutions, and denote by  $\Delta f_a$ ,  $\Delta f_d$ , and  $\Delta t_m$  the increments to the next approximation. In the first order,

the three equations become:

$$\begin{aligned}
x_m &= P(x_a, x_b, x_c, x_d, t_m) + \Delta f_a \cdot T_{ax} \cdot 3t_m(1 - t_m)^2 + \Delta f_d \cdot T_{dx} \cdot 3t_m^2(1 - t_m) \\
&\quad + \Delta t_m \frac{\partial}{\partial t_m} P(x_a, x_b, x_c, x_d, t_m) \\
y_m &= P(y_a, y_b, y_c, y_d, t_m) + \Delta f_a \cdot T_{ay} \cdot 3t_m(1 - t_m)^2 + \Delta f_d \cdot T_{dy} \cdot 3t_m^2(1 - t_m) \\
&\quad + \Delta t_m \frac{\partial}{\partial t_m} P(y_a, y_b, y_c, y_d, t_m) \\
&\quad \left( \frac{\partial}{\partial t_m} P(x_a, x_b, x_c, x_d, t_m) + \Delta f_a \cdot T_{ax} \cdot 3(1 - 4t_m + 3t_m^2) + \Delta f_d \cdot T_{dx} \cdot 3(2t_m - 3t_m^2) \right. \\
&\quad \left. + \Delta t_m \cdot 6((x_a - 2x_b + x_c) + t_m(x_d - x_a + 3(x_b - x_c))) \right) \cdot T_{my} \\
&= \left( \frac{\partial}{\partial t_m} P(y_a, y_b, y_c, y_d, t_m) + \Delta f_a \cdot T_{ay} \cdot 3(1 - 4t_m + 3t_m^2) + \Delta f_d \cdot T_{dy} \cdot 3(2t_m - 3t_m^2) \right. \\
&\quad \left. + \Delta t_m \cdot 6((y_a - 2y_b + y_c) + t_m(y_d - y_a + 3(y_b - y_c))) \right) \cdot T_{mx}
\end{aligned}$$

Rewrite the equations so that they resemble the T<sub>E</sub>X code.

$$\begin{aligned}
8P(x_a, x_b, x_c, x_d, t_m) - 8x_m &= -\Delta f_a \cdot 3T_{ax} \cdot 2t_m \cdot (2(1 - t_m))^2 \\
&\quad - \Delta f_d \cdot 3T_{dx} \cdot 4t_m^2 \cdot 2(1 - t_m) - \Delta t_m \cdot 8 \frac{\partial}{\partial t_m} P(x_a, x_b, x_c, x_d, t_m) \\
8P(y_a, y_b, y_c, y_d, t_m) - 8y_m &= -\Delta f_a \cdot 3T_{ay} \cdot 2t_m \cdot (2(1 - t_m))^2 \\
&\quad - \Delta f_d \cdot 3T_{dy} \cdot 4t_m^2 \cdot 2(1 - t_m) - \Delta t_m \cdot 8 \frac{\partial}{\partial t_m} P(y_a, y_b, y_c, y_d, t_m) \\
T_{mx} \cdot 8 \frac{\partial}{\partial t_m} P(y_a, y_b, y_c, y_d, t_m) - T_{my} \cdot 8 \frac{\partial}{\partial t_m} P(x_a, x_b, x_c, x_d, t_m) \\
&= -\Delta f_a \cdot (3T_{ay} \cdot 2T_{mx} - 3T_{ax} \cdot 2T_{my}) \cdot 2(1 - 3t_m) \cdot 2(1 - t_m) \\
&\quad - \Delta f_d \cdot (3T_{dy} \cdot 2T_{mx} - 3T_{dx} \cdot 2T_{my}) \cdot 2(2 - 3t_m) \cdot 2t_m \\
&\quad - \Delta t_m \cdot (((y_d - y_a + 3(y_b - y_c)) \cdot 2t_m + 2(y_a - 2y_b + y_c)) \cdot 3 \cdot 8T_{mx} \\
&\quad - ((x_d - x_a + 3(x_b - x_c)) \cdot 2t_m + 2(x_a - 2x_b + x_c)) \cdot 3 \cdot 8T_{my})
\end{aligned}$$

Substitute  $2t_m = \tau_m$ .

$$\begin{aligned}
8P(x_a, x_b, x_c, x_d, t_m) - 8x_m &= -\Delta f_a \cdot 3T_{ax} \cdot \tau_m(2 - \tau_m)^2 \\
&\quad - \Delta f_d \cdot 3T_{dx} \cdot \tau_m^2(2 - \tau_m) - \frac{1}{2}\Delta\tau_m \cdot 8 \frac{\partial}{\partial t_m} P(x_a, x_b, x_c, x_d, t_m) \\
8P(y_a, y_b, y_c, y_d, t_m) - 8y_m &= -\Delta f_a \cdot 3T_{ay} \cdot \tau_m \cdot (2 - \tau_m)^2 \\
&\quad - \Delta f_d \cdot 3T_{dy} \cdot \tau_m^2(2 - \tau_m) - \frac{1}{2}\Delta\tau_m \cdot 8 \frac{\partial}{\partial t_m} P(y_a, y_b, y_c, y_d, t_m) \\
T_{mx} \cdot 8 \frac{\partial}{\partial t_m} P(y_a, y_b, y_c, y_d, t_m) - T_{my} \cdot 8 \frac{\partial}{\partial t_m} P(x_a, x_b, x_c, x_d, t_m) \\
&= -\Delta f_a \cdot (3T_{ay} \cdot 2T_{mx} - 3T_{ax} \cdot 2T_{my}) \cdot (2 - 3\tau_m)(2 - \tau_m) \\
&\quad - \Delta f_d \cdot (3T_{dy} \cdot 2T_{mx} - 3T_{dx} \cdot 2T_{my}) \cdot (4 - 3\tau_m)\tau_m \\
&\quad - \Delta\tau_m \cdot (((y_d - y_a + 3(y_b - y_c)) \cdot \tau_m + 2(y_a - 2y_b + y_c)) \cdot 12T_{mx} \\
&\quad - ((x_d - x_a + 3(x_b - x_c)) \cdot \tau_m + 2(x_a - 2x_b + x_c)) \cdot 12T_{my})
\end{aligned}$$

The translation into T<sub>E</sub>X dimensions:

- $f_a = \text{\xP@fa}$ ,  $f_d = \text{\xP@fd}$
- $\tau_m = \text{\xP@tm}$
- $x_a = \text{\xP@xa}, \dots, x_d = \text{\xP@xd}, \dots, y_d = \text{\xP@yd}$
- $8P(x_1, x_2, x_3, x_4, \frac{1}{2}x_5) = \text{\xP@bezierpoly\#1\#2\#3\#4\#5}$
- $8x_m = \text{\xP@xm}$ ,  $8y_m = \text{\xP@ym}$

- $3T_{ax} = \text{\xP@Tax}, 3T_{dx} = \text{\xP@Tdx}, 3T_{ay} = \text{\xP@Tay}, 3T_{dy} = \text{\xP@Tdy}$
- $8\frac{\partial}{\partial x_5}P(x_1, x_2, x_3, x_4, \frac{1}{2}x_5) = \text{\xP@beziertan\#1\#2\#3\#4\#5}$

Temporary:

- $2 - \tau_m = \text{\xP@ta}$
- $\tau_m(2 - \tau_m) = \text{\xP@tb}$
- $T_{mx} = \text{\xP@Tmx}, T_{my} = \text{\xP@Tmy}$
- $2 - 3\tau_m = \text{\xP@tb}$
- $4 - 3\tau_m = \text{\xP@tc}$

Since the linear system above tends to be singular or ill-conditioned (think about the frequent case when all control points are nearly collinear!), the Gauss algorithm `\xP@solvelinearsystem` does not always return a valid solution. In these cases, the system is not solved exactly but approximated iteratively in `\xP@applinsys`.

```

\xP@tmx
\xP@tmy 664 \ifdefinable\xP@tmx\relax
        665 \ifdefinable\xP@tmy\relax

\xP@Tmxy ●4
\xP@Tmyx 666 \newcommand*\xP@Tmxy{* \xP@Tmx / \xP@Tmy}
        667 \newcommand*\xP@Tmyx{* \xP@Tmy / \xP@Tmx}

\xP@Tmzero
        668 \newcommand*\xP@Tmzero{* \z@}

\xP@offsetsegment ●1 ●3 ●4 Offset a cubic segment. The offset distance is given in \xP@off. The anchor points
are given in \X@p,...,\Y@c. The new Bézier curve is returned in \xP@xa,...,\xP@yd.
669 \newcommand*\xP@offsetsegment{%
Initial guesses for the tangent vector scalings \xP@fa, \xP@fd and the near-middle position
\xP@tm
670 \xP@fa\p@
671 \xP@fd\p@
672 \xP@tm\p@
8 times (middle point plus offset)
673 \xP@normalvec{.5pt}\xP@off
674 \xP@xm\dimexpr(\X@p+\X@c+(\L@c+\R@c)*3)+8\d@X\relax
675 \xP@ym\dimexpr(\Y@p+\Y@c+(\U@c+\D@c)*3)+8\d@Y\relax
New first anchor point
676 \xP@normalvec\z@\xP@off
677 \xP@xa\dimexpr\X@p+\d@X\relax
678 \xP@ya\dimexpr\Y@p+\d@Y\relax
New last anchor point
679 \xP@normalvec\p@\xP@off
680 \xP@xd\dimexpr\X@c+\d@X\relax
681 \xP@yd\dimexpr\Y@c+\d@Y\relax
Tangent vector at 0. This also handles degenerate cases.
682 \xP@Tax\dimexpr\L@c-\X@p\relax
683 \xP@Tay\dimexpr\U@c-\Y@p\relax
684 \ifdim\xP@Tax=\z@
685 \ifdim\xP@Tay=\z@
686 \xP@Tax\dimexpr\R@c-\X@p\relax
687 \xP@Tay\dimexpr\D@c-\Y@p\relax

```

```

688     \ifdim\xP@Tax=\z@
689     \ifdim\xP@Tay=\z@
690     \xP@Tax\dimexpr\X@c-\X@p\relax
691     \xP@Tay\dimexpr\Y@c-\Y@p\relax
692     \fi
693     \fi
694     \fi
695     \fi
696     \multiply\xP@Tax\thr@@
697     \multiply\xP@Tay\thr@@

```

Tangent vector at 1.

```

698     \xP@Tdx\dimexpr\R@c-\X@c\relax
699     \xP@Tdy\dimexpr\D@c-\Y@c\relax
700     \ifdim\xP@Tdx=\z@
701     \ifdim\xP@Tdy=\z@
702     \xP@Tdx\dimexpr\L@c-\X@c\relax
703     \xP@Tdy\dimexpr\U@c-\Y@c\relax
704     \ifdim\xP@Tdx=\z@
705     \ifdim\xP@Tdy=\z@
706     \xP@Tdx\dimexpr\X@p-\X@c\relax
707     \xP@Tdy\dimexpr\Y@p-\Y@c\relax
708     \fi
709     \fi
710     \fi
711     \fi
712     \multiply\xP@Tdx\thr@@
713     \multiply\xP@Tdy\thr@@

```

The main loop for finding the offset curve

```

714     \count@\z@
715     \loop
716     \@tempswafalse

```

At most 10 iterations

```

717     \ifnum10>\count@

```

Set the new control points up.

```

718     \xP@offsetpoints

```

Determine the quality of the approximation by an objective function.

```

719     \xP@objfun\xP@oldobj
720     \ifdim\xP@oldobj>\xP@maxobjfun\relax\@tempswatrue\fi
721     \fi
722     \if@tempswa
723     \xP@offsetloop
724     \repeat

```

Return the new anchor points.

```

725     \xdef\@gtempa{\X@p\the\xP@xa\Y@p\the\xP@ya
726     \L@c\the\xP@xb\U@c\the\xP@yb\R@c\the\xP@xc\D@c\the\xP@yc
727     \X@c\the\xP@xd\Y@c\the\xP@yd\relax}%
728     }%
729     \@gtempa
730 }

```

\xP@offsetloop ●134 The iteration in the offset loop: set up and solve (or approximate) the linear system.

```

731 \newcommand*\xP@offsetloop{%
732   \xP@C\dimexpr\xP@C/2\relax
733   \xP@G\dimexpr\xP@G/2\relax

```



1st linear equation

```
734 \xP@ta\dimexpr2\p@-\xP@tm\relax
735 \xP@tb\dimexpr\xP@tm*\xP@ta/\p@\relax
736 \xP@A\dimexpr\xP@Tax*\xP@tb/\p@*\xP@ta/\p@\relax
737 \xP@B\dimexpr\xP@Tdx*\xP@tb/\p@*\xP@tm/\p@\relax
```

2nd linear equation

```
738 \xP@E\dimexpr\xP@Tay*\xP@tb/\p@*\xP@ta/\p@\relax
739 \xP@F\dimexpr\xP@Tdy*\xP@tb/\p@*\xP@tm/\p@\relax
```

3rd linear equation

```
740 \xP@tb\dimexpr2\p@-3\xP@tm\relax
741 \xP@tc\dimexpr\xP@tb+2\p@\relax
742 \xP@I\dimexpr(2\xP@Tay\xP@tmx-2\xP@Tax\xP@tmy)
743 *\xP@tb/\p@*\xP@ta/\p@\relax
744 \xP@J\dimexpr(2\xP@Tdy\xP@tmx-2\xP@Tdx\xP@tmy)
745 *\xP@tc/\p@*\xP@tm/\p@\relax
746 \xP@K\dimexpr((\xP@yd-\xP@ya+(\xP@yb-\xP@yc)*3)
747 *\xP@tm/\p@+(\xP@yc-2\xP@yb+\xP@ya)*2)*12\xP@tmx
748 -((\xP@xd-\xP@xa+(\xP@xb-\xP@xc)*3)
749 *\xP@tm/\p@+(\xP@xc-2\xP@xb+\xP@xa)*2)*12\xP@tmy\relax
```

Solve the system.

```
750 \xP@solvelinearsystem
751 \ifxP@validsol
```

Check whether the result is feasible and whether it actually improves the approximation.

```
752 \xP@correctsol
753 \ifdim\xP@ta=\z@
754 \ifdim\xP@tb=\z@
755 \ifdim\xP@tc=\z@
756 \xP@validsolfalse
757 \fi\fi\fi
758 \fi
```

If the exact solution is not valid, try to at least approximate a solution.

```
759 \ifxP@validsol
760 \else
761 \xP@applinsys
```

This time, the solution is not checked but applied immediately.

```
762 \advance\xP@fa-\xP@ta
763 \advance\xP@fd-\xP@tb
764 \advance\xP@tm-\xP@tc
```

The near-middle parameter on the curve must not lie outside the segment.

```
765 \ifdim\xP@tm<\z@\xP@tm\z@\fi
766 \ifdim\xP@tm>\tw@\p@\xP@tm\tw@\p@\fi
767 \fi
768 \advance\count@\@ne
769 }
```

\xP@maxsol Heuristic: maximal solution so that no arithmetic overflow is produced.

```
770 \newcommand*\xP@maxsol{3pt}
```

\xP@correctsol ●3 ●4 Check whether the solution is feasible and actually improves the objective function.

```
771 \newcommand*\xP@correctsol{%
```

If the solution is too big, scale all variables uniformly.

```
772 \xP@M\z@
773 \xP@Max\xP@M\xP@ta
774 \xP@Max\xP@M\xP@tb
775 \xP@Max\xP@M\xP@tc
776 \ifdim\xP@M>\xP@maxsol
```

```

777 \xP@ta\dimexpr\xP@maxsol*\xP@ta/\xP@M\relax
778 \xP@tb\dimexpr\xP@maxsol*\xP@tb/\xP@M\relax
779 \xP@tc\dimexpr\xP@maxsol*\xP@tc/\xP@M\relax
780 \fi

```

Apply the solution. Save the old value of `\xP@tm` to be able to restore it.

```

781 \advance\xP@fa-\xP@ta
782 \advance\xP@fd-\xP@tb
783 \xP@M\xP@tm
784 \advance\xP@tm-\xP@tc

```

The near-middle parameter must lie on the segment.

```

785 \ifdim\xP@tm<\z@\xP@tm\z@\fi
786 \ifdim\xP@tm>\tw@\p@\xP@tm\tw@\p@\fi

```

Check whether the solution actually improves the objective function.

```

787 {%
788 \xP@offsetpoints
789 \xP@objfun\xP@M
790 \expandafter}%

```

If not, restore the old values and declare the solution invalid.

```

791 \ifdim\xP@M>\xP@oldobj
792 \advance\xP@fa\xP@ta
793 \advance\xP@fd\xP@tb
794 \xP@tm\xP@M
795 \xP@validsolfalse
796 \fi
797 }

```

`\xP@objfun` ●3 ●4 The objective function: sum of squares of the deviation in  $x$ - and  $y$ -direction and the angular deviation at the middle point. We also compute some terms which will be used in the linear system.

```

798 \newcommand*\xP@objfun[1]{%
799 \xP@D\xP@bezierpoly\xP@xa\xP@xb\xP@xc\xP@xd\xP@tm
800 \xP@D\dimexpr\xP@D-\xP@xm\relax
801 \xP@H\xP@bezierpoly\xP@ya\xP@yb\xP@yc\xP@yd\xP@tm
802 \xP@H\dimexpr\xP@H-\xP@ym\relax
803 \xP@Tmx\dimexpr\X@p-\X@c+\L@c-\R@c\relax
804 \xP@Tmy\dimexpr\Y@p-\Y@c+\U@c-\D@c\relax
805 \xP@ifabsless\xP@Tmy\xP@Tmx
806 \let\xP@tmy\xP@Tmyx
807 \let\xP@tmx\empty
808 \else
809 \ifdim\xP@Tmy=\z@
810 \let\xP@tmx\xP@Tmzero
811 \let\xP@tmy\xP@Tmzero
812 \else
813 \let\xP@tmy\empty
814 \let\xP@tmx\xP@Tmxy
815 \fi
816 \fi
817 \xP@C\xP@beziertan\xP@xa\xP@xb\xP@xc\xP@xd\xP@tm
818 \xP@G\xP@beziertan\xP@ya\xP@yb\xP@yc\xP@yd\xP@tm
819 \xP@L\dimexpr\xP@G\xP@tmx-\xP@C\xP@tmy\relax

```

If the deviation is too big, let the objective function be `\maxdimen`. Otherwise, compute the sum of squares.

```

820 #1\z@
821 \xP@Max#1\xP@D
822 \xP@Max#1\xP@H
823 \xP@Max#1\xP@L
824 \ifdim#1>4843165sp

```

```

825     #1\maxdimen
826   \else
827     #1\dimexpr\xP@D*\xP@D/\p@+\xP@H*\xP@H/\p@+\xP@L*\xP@L/\p@\relax
828   \fi
829 }

```

`\xP@offsetpoints` ●3 ●4 Compute the new control points from the factors `\xP@fa`, `\xP@fd`.

```

830 \newcommand*\xP@offsetpoints{%
831   \xP@xb\dimexpr\xP@xa+\xP@Tax*\xP@fa/196608\relax
832   \xP@yb\dimexpr\xP@ya+\xP@Tay*\xP@fa/196608\relax
833   \xP@xc\dimexpr\xP@xd+\xP@Tdx*\xP@fd/196608\relax
834   \xP@yc\dimexpr\xP@yd+\xP@Tdy*\xP@fd/196608\relax
835 }

```

`\xP@bezierpoly` Formula for the polynomial  $8 \left( \#1 \cdot (1-t)^3 + 3 \cdot \#2 \cdot t(1-t)^2 + 3 \cdot \#3 \cdot t^2(1-t) + \#4 \cdot t^3 \right)$ ,  $t = \frac{1}{2}\#5$ .

```

836 \newcommand*\xP@bezierpoly[5]{%
837   \dimexpr(((\#4-\#1+(\#2-\#3)*3)*\#5/\p@+(\#1-2\#2+\#3)*6)*\#5/\p@+(\#2-\#1)*12)*\#5/\p@
838   +\#1*8\relax
839 }

```

`\xP@beziertan` Formula for the polynomial

$$24 \left( -\#1 \cdot (1-t)^2 + \#2 \cdot (3t^2 - 4t + 1) + \#3 \cdot (-3t^2 + 2t) + \#4 \cdot t^2 \right), \quad t = \frac{1}{2}\#5.$$

Up to a scalar factor, this is the derivative of the third order Bézier polynomial above.

```

840 \newcommand*\xP@beziertan[5]{%
841   \dimexpr((\#4-\#1+(\#2-\#3)*3)*3*\#5/32768+(\#1-2\#2+\#3)*24)*\#5/\p@+(\#2-\#1)*24\relax
842 }

```

`\xP@solvelinearsystem` ●3 The macro `\xP@solvelinearsystem` solves a system of three linear equations by the Gauss algorithm. The coefficients and desired values are passed in the extended matrix

$$\left( \begin{array}{ccc|c} \xP@A & \xP@B & \xP@C & \xP@D \\ \xP@E & \xP@F & \xP@G & \xP@H \\ \xP@I & \xP@J & \xP@K & \xP@L \end{array} \right)$$

The solution is returned in the vector  $(\xP@ta, \xP@tb, \xP@tc)$ .

`\xP@varone` `\xP@vartwo` With column swapping in the Gauss algorithm, variable names might be changed. These macros record the variables.

```

843 \ifdefinable\xP@varone\relax
844 \ifdefinable\xP@vartwo\relax
845 \ifdefinable\xP@varthree\relax

```

`\ifxP@validsol` Records if a valid solution to the linear system is returned.

```

846 \newif\ifxP@validsol

847 \newcommand*\xP@solvelinearsystem{%
Scale the matrix so that the highest absolute value in each row and each column is  $\geq 2048\text{pt}$ 
and  $< 4096\text{pt}$ .
848   \xP@scalerow\xP@A\xP@B\xP@C\xP@D
849   \xP@scalerow\xP@E\xP@F\xP@G\xP@H
850   \xP@scalerow\xP@I\xP@J\xP@K\xP@L
851   \xP@scalectol\xP@A\xP@E\xP@I\xP@scalectwo
852   \xP@scalectol\xP@B\xP@F\xP@J\xP@scalectwo
853   \xP@scalectol\xP@C\xP@G\xP@K\xP@scalecthree

Record the initial variable-to-column assignment.
854   \let\xP@varone\xP@ta
855   \let\xP@vartwo\xP@tb
856   \let\xP@varthree\xP@tc

```

Find the pivot position. \xPQM is used temporarily.

```

857 \count@\m@ne
858 \@tempcnta@m@ne
859 \xP@ifabsless\xP@A\xP@B\@tempcnta\z@\xPQM\xP@B
860 \else\xPQM\xP@A\fi
861 \xP@ifabsless\xPQM\xP@C\@tempcnta\@ne\xPQM\xP@C\fi
862 \xP@ifabsless\xPQM\xP@E\@tempcnta@m@ne\count@\z@\xPQM\xP@E\fi
863 \xP@ifabsless\xPQM\xP@F\@tempcnta\z@\count@\z@\xPQM\xP@F\fi
864 \xP@ifabsless\xPQM\xP@G\@tempcnta\@ne\count@\z@\xPQM\xP@G\fi
865 \xP@ifabsless\xPQM\xP@I\@tempcnta@m@ne\count@\@ne\xPQM\xP@I\fi
866 \xP@ifabsless\xPQM\xP@J\@tempcnta\z@\count@\@ne\xPQM\xP@J\fi
867 \xP@ifabsless\xPQM\xP@K\@tempcnta\@ne\count@\@ne\fi

```

Swap rows

```

868 \ifcase\count@
869 \xP@swapdim\xP@A\xP@E
870 \xP@swapdim\xP@B\xP@F
871 \xP@swapdim\xP@C\xP@G
872 \xP@swapdim\xP@D\xP@H
873 \or
874 \xP@swapdim\xP@A\xP@I
875 \xP@swapdim\xP@B\xP@J
876 \xP@swapdim\xP@C\xP@K
877 \xP@swapdim\xP@D\xP@L
878 \fi

```

Swap columns

```

879 \ifcase\@tempcnta
880 \xP@swapdim\xP@A\xP@B
881 \xP@swapdim\xP@E\xP@F
882 \xP@swapdim\xP@I\xP@J
883 \let\xP@varone\xP@tb
884 \let\xP@vartwo\xP@ta
885 \xP@swapnum\xP@scaleone\xP@scaletwo
886 \or
887 \xP@swapdim\xP@A\xP@C
888 \xP@swapdim\xP@E\xP@G
889 \xP@swapdim\xP@I\xP@K
890 \let\xP@varone\xP@tc
891 \let\xP@varthree\xP@ta
892 \xP@swapnum\xP@scaleone\xP@scalethree
893 \fi

```

First elimination

```

894 \multiply\xP@E@m@ne
895 \multiply\xP@I@m@ne

```

Absolute values below are < 8192pt.

```

896 \advance\xP@F\dimexpr\xP@B*\xP@E/\xP@A\relax
897 \advance\xP@G\dimexpr\xP@C*\xP@E/\xP@A\relax
898 \advance\xP@H\dimexpr\xP@D*\xP@E/\xP@A\relax
899 \advance\xP@J\dimexpr\xP@B*\xP@I/\xP@A\relax
900 \advance\xP@K\dimexpr\xP@C*\xP@I/\xP@A\relax
901 \advance\xP@L\dimexpr\xP@D*\xP@I/\xP@A\relax

```

Find the second pivot element. \xPQM is used temporarily.

```

902 \count@\m@ne
903 \xP@ifabsless\xP@F\xP@G\@tempcnta\z@\xPQM\xP@G
904 \else\@tempcnta@m@ne\xPQM\xP@F\fi
905 \xP@ifabsless\xPQM\xP@J\@tempcnta@m@ne\count@\z@\xPQM\xP@J\fi
906 \xP@ifabsless\xPQM\xP@K\@tempcnta\z@\count@\z@\fi

```

Swap rows

```

907 \ifnum\count@=\z@
908 \xP@swapdim\xP@F\xP@J
909 \xP@swapdim\xP@G\xP@K
910 \xP@swapdim\xP@H\xP@L
911 \fi

```

Swap columns

```

912 \ifnum\@tempcnta=\z@
913 \xP@swapdim\xP@B\xP@C
914 \xP@swapdim\xP@F\xP@G
915 \xP@swapdim\xP@J\xP@K
916 \let\@tempa\xP@varthree
917 \let\xP@varthree\xP@vartwo
918 \let\xP@vartwo\@tempa
919 \xP@swapnum\xP@scaletwo\xP@scaletthree
920 \fi

```

Second elimination. Absolute values are  $< 16384$ pt.

```

921 \advance\xP@K\dimexpr-\xP@G*\xP@J/\xP@F\relax
922 \advance\xP@L\dimexpr-\xP@H*\xP@J/\xP@F\relax

```

Compute the result from the upper triangular form. Since the matrix can be singular, we have to ensure in every step that no overflow occurs. In general, we do not allow any solution greater than 60pt.

```

923 \xP@ifabsless{\dimexpr\xP@L/60\relax}{\dimexpr\xP@K/\xP@scaletthree\relax}%
924 \xP@validsoltrue
925 \xP@varthree\dimexpr\xP@L*(\xP@scaletthree*\p@)/\xP@K\relax
926 \else
927 \xP@validsolfalse
928 \fi
929 \xP@checkabs{\xP@H/8191}{\xP@F/\xP@scalettwo}%
930 \xP@checkabs{\xP@G/\xP@scaletthree/136}{\xP@F/\xP@scalettwo}%
931 \ifxP@validsol
932 \xP@vartwo\dimexpr\xP@H*(\xP@scalettwo*\p@)/\xP@F
933 -\xP@varthree*\xP@scalettwo/\xP@scaletthree*\xP@G/\xP@F\relax
934 \xP@checkabs\xP@vartwo{60pt}%
935 \fi
936 \xP@checkabs{\xP@D/5461}{\xP@A/\xP@scaleone}%
937 \xP@checkabs{\xP@B/\xP@scalettwo/91}{\xP@A/\xP@scaleone}%
938 \xP@checkabs{\xP@C/\xP@scaletthree/91}{\xP@A/\xP@scaleone}%
939 \ifxP@validsol
940 \xP@varone\dimexpr\xP@D*(\xP@scaleone*\p@)/\xP@A
941 -\xP@vartwo*\xP@scaleone/\xP@scalettwo*\xP@B/\xP@A
942 -\xP@varthree*\xP@scaleone/\xP@scaletthree*\xP@C/\xP@A\relax
943 \xP@checkabs\xP@varone{60pt}%
944 \fi

```

Return the result.

```

945 \xdef\@gtempa{%
946 \ifxP@validsol
947 \xP@ta\the\xP@ta\relax
948 \xP@tb\the\xP@tb\relax
949 \xP@tc\the\xP@tc\relax
950 \noexpand\xP@validsoltrue
951 \else
952 \noexpand\xP@validsolfalse
953 \fi
954 }%
955 }\@gtempa
956 }

```

**\xP@scalerow**  Scale a row of the matrix to improve numerical precision. We scale by a power of two such that the maximal length is between 2048pt and 4096pt.

```

957 \newcommand*\xP@scalerow[4]{%
958   \xP@M\z@
959   \xP@Max\xP@M#1%
960   \xP@Max\xP@M#2%
961   \xP@Max\xP@M#3%
962   \xP@Max\xP@M#4%
134217727 = 2048 · 65536 − 1
963   \count@134217727
964   \loop
965     \divide\xP@M\tw@
966   \ifdim\xP@M>\z@
967     \divide\count@\tw@
968   \repeat
969   \advance\count@\@ne
970   \multiply#1\count@
971   \multiply#2\count@
972   \multiply#3\count@
973   \multiply#4\count@
974 }

```

`\xP@scalecol` ●3 Scale a column of the matrix to improve numerical precision. The scaling factor has to be recorded for the solution assignment later.

```

975 \newcommand*\xP@scalecol[4]{%
976   \xP@M\z@
977   \xP@Max\xP@M#1%
978   \xP@Max\xP@M#2%
979   \xP@Max\xP@M#3%
16777215 = 2048 · 8192 − 1
980   #416777215
981   \loop
982     \divide\xP@M\tw@
983   \ifdim\xP@M>\z@
984     \divide#4\tw@
985   \repeat
986   \advance#4\@ne
987   \multiply#1#4%
988   \multiply#2#4%
989   \multiply#3#4%
990 }

```

`\xP@checkabs`

```

991 \newcommand*\xP@checkabs[2]{%
992   \xP@ifabsless{\dimexpr#1\relax}{\dimexpr#2\relax}\else\xP@validsolfalse\fi}

```

`\xP@applinsys` ●1 ●3 ●6 This is the second, alternative algorithm for Newton's method in the offset algorithm. Approximate a solution  $x$  for the linear system  $Ax = b$  for a  $(3 \times 3)$ -matrix  $A$ . The aim is to make the norm  $\|Ax - b\|$  small with small values of  $\|x\|$ . The approach: Set  $x = \lambda A^t b$  since the normed scalar product  $\langle Ax, b \rangle / \|x\|$  is maximal in this case. The norm  $\|Ax - b\|$  is then minimal for  $\lambda = \|A^t b\|^2 / \|AA^t b\|^2$ .

This approximation is performed between one and three times.

```

993 \newcommand*\xP@applinsys{%

```

First iteration: approximate a solution and record the result.

```

994   \xP@applinsys@
995   \xP@ta\xP@dta
996   \xP@tb\xP@dtb
997   \xP@tc\xP@dtc

```

If the result is nonzero...

```

998   \xP@checkapp
999   \if@tempswa

```

...modify the objective function by the estimated change, approximate again,...

```

1000 \xP@modobj
1001 \xP@applinsys@
...and test for a nonzero result. If it is nonzero, repeat it a third time.
1002 \xP@checkapp
1003 \if@tempswa
1004 \xP@modsol
1005 \xP@modobj
1006 \xP@applinsys@
1007 \xP@modsol
1008 \fi
1009 \fi

```

Return the accumulated approximation from one to three iterations.

```

1010 \xdef\@gtempa{%
1011 \xP@ta\the\xP@ta\relax
1012 \xP@tb\the\xP@tb\relax
1013 \xP@tc\the\xP@tc\relax
1014 }\@gtempa
1015 }

```

\xP@checkapp •6 Check whether the solution is nonzero.

```

1016 \newcommand*\xP@checkapp{%
1017 \@tempswatrue
1018 \ifdim\xP@dta=\z@
1019 \ifdim\xP@dtb=\z@
1020 \ifdim\xP@dtc=\z@
1021 \@tempswafalse
1022 \fi\fi\fi
1023 }

```

\xP@modobj •3 •6 Modify the objective function by the estimated difference, according to the first-order approximation.

```

1024 \newcommand*\xP@modobj{%
1025 \advance\xP@D
1026 \dimexpr-\xP@A*\xP@dta/\p@-\xP@B*\xP@dtb/\p@-\xP@C*\xP@dtc/\p@\relax
1027 \advance\xP@H
1028 \dimexpr-\xP@E*\xP@dta/\p@-\xP@F*\xP@dtb/\p@-\xP@G*\xP@dtc/\p@\relax
1029 \advance\xP@L
1030 \dimexpr-\xP@I*\xP@dta/\p@-\xP@J*\xP@dtb/\p@-\xP@K*\xP@dtc/\p@\relax
1031 }

```

\xP@modsol •3 •6 Modify the solution vector by the approximation.

```

1032 \newcommand*\xP@modsol{%
1033 \advance\xP@ta\xP@dta
1034 \advance\xP@tb\xP@dtb
1035 \advance\xP@tc\xP@dtc
1036 }

```

\xP@applinsys@ •1 •3 •6 The heart of the approximation routine.

```

1037 \newcommand*\xP@applinsys@{%

```

Determine scaling factors \xP@sa and \xP@sb to improve numerical precision.

```

1038 \xP@sa\z@
1039 \xP@Max\xP@sa\xP@A
1040 \xP@Max\xP@sa\xP@B
1041 \xP@Max\xP@sa\xP@C
1042 \xP@Max\xP@sa\xP@E
1043 \xP@Max\xP@sa\xP@F
1044 \xP@Max\xP@sa\xP@G

```

```

1045 \xP@Max\xP@sa\xP@I
1046 \xP@Max\xP@sa\xP@J
1047 \xP@Max\xP@sa\xP@K
1048 \xP@sa\ifdim\xP@sa<5460pt\thr@@\xP@sa\else\maxdimen\fi
1049 \xP@sb\z@
1050 \xP@Max\xP@sb\xP@D
1051 \xP@Max\xP@sb\xP@H
1052 \xP@Max\xP@sb\xP@L

Scale the vector  $b$ .
1053 \ifdim\xP@sb>\z@
1054 \xP@D\dimexpr\xP@D*\maxdimen/\xP@sb\relax
1055 \xP@H\dimexpr\xP@H*\maxdimen/\xP@sb\relax
1056 \xP@L\dimexpr\xP@L*\maxdimen/\xP@sb\relax
1057 \fi

Vector  $A^t b$  (scaled)
1058 \xP@Aba\dimexpr\xP@A*\xP@D/\xP@sa+\xP@E*\xP@H/\xP@sa
1059 +\xP@I*\xP@L/\xP@sa\relax
1060 \xP@Abb\dimexpr\xP@B*\xP@D/\xP@sa+\xP@F*\xP@H/\xP@sa
1061 +\xP@J*\xP@L/\xP@sa\relax
1062 \xP@Abc\dimexpr\xP@C*\xP@D/\xP@sa+\xP@G*\xP@H/\xP@sa
1063 +\xP@K*\xP@L/\xP@sa\relax

Vector  $AA^t b$  (scaled)
1064 \xP@AAba\dimexpr\xP@A*\xP@Aba/\xP@sa+\xP@B*\xP@Abb/\xP@sa
1065 +\xP@C*\xP@Abc/\xP@sa\relax
1066 \xP@AAb\dimexpr\xP@E*\xP@Aba/\xP@sa+\xP@F*\xP@Abb/\xP@sa
1067 +\xP@G*\xP@Abc/\xP@sa\relax
1068 \xP@AAbc\dimexpr\xP@I*\xP@Aba/\xP@sa+\xP@J*\xP@Abb/\xP@sa
1069 +\xP@K*\xP@Abc/\xP@sa\relax

Another scaling factor.
1070 \xP@sc\z@
1071 \xP@Max\xP@sc\xP@Aba
1072 \xP@Max\xP@sc\xP@Abb
1073 \xP@Max\xP@sc\xP@Abc
1074 \xP@Max\xP@sc\xP@AAba
1075 \xP@Max\xP@sc\xP@AAb
1076 \xP@Max\xP@sc\xP@AAbc

 $\|A^t b\|^2$  and  $\|AA^t b\|^2$ 
1077 \ifdim\xP@sc=\z@
1078 \xP@AAb\z@
1079 \else
1080 \xP@Ab\dimexpr\xP@Aba*\xP@bigdim/\xP@sc*\xP@Aba/\xP@sc
1081 +\xP@Abb*\xP@bigdim/\xP@sc*\xP@Abb/\xP@sc
1082 +\xP@Abc*\xP@bigdim/\xP@sc*\xP@Abc/\xP@sc
1083 \relax
1084 \xP@AAb\dimexpr\xP@AAba*\xP@bigdim/\xP@sc*\xP@AAb/\xP@sc
1085 +\xP@AAb*\xP@bigdim/\xP@sc*\xP@AAb/\xP@sc
1086 +\xP@AAbc*\xP@bigdim/\xP@sc*\xP@AAbc/\xP@sc
1087 \relax
1088 \fi

The approximation  $x = \lambda A^t b$  with  $\lambda = \|A^t b\|^2 / \|AA^t b\|^2$ .
1089 \xdef\@gtempa{%
1090 \ifdim\xP@AAb=\z@
1091 \xP@dta\z@
1092 \xP@dtb\z@
1093 \xP@dtc\z@
1094 \else
1095 \xP@dta\the\dimexpr\xP@Aba*\xP@sb/\xP@sa*\p@/\xP@AAb*\xP@Ab/\maxdimen

```



```

1096      \relax
1097      \xP@dtb\the\dimexpr\xP@Abb*\xP@sb/\xP@sa*\p@/\xP@AAb*\xP@Ab/\maxdimen
1098      \relax
1099      \xP@dtc\the\dimexpr\xP@Abc*\xP@sb/\xP@sa*\p@/\xP@AAb*\xP@Ab/\maxdimen
1100      \relax
1101      \fi
1102    }%
1103    }\@gtempa
1104 }

```

\ifxP@offsetok Switch whether the offset curve is enough

```
1105 \newif\ifxP@offsetok
```

\xP@maxdev Maximal deviation, measured at 19 points on the curve. The actual tolerance is  $1/8$  of \xP@maxdev. With the current value 0.1pt, the tolerance is 0.0125pt, which is about  $1/32$  of the line width for the Computer Modern fonts.

```
1106 \newcommand*\xP@maxdev{.1\p@}
```

\xP@maxobjfun Tolerance for the objective function. Recommended value is  $\frac{1}{2}(\xP@maxdev)^2$ .

```
1107 \newcommand*\xP@maxobjfun{.005\p@}
```

\xP@testoffset ● ● ● Test procedure for the offset curve. It tests whether the Bézier curve defined by the control points \X@p,...,\Y@c is a good approximation for the offset curve of the partial curve defined by \xP@xa,...,\xP@yd in the parameter interval  $[\xP@a, \xP@b] \subseteq [0pt, \xP@bigdim]$ . The parameter interval is uniformly divided by 20, and the deviation is measured at the 19 inner positions. (Since the boundary points are offset exactly by the algorithm, they do not need to be checked.)

For simplicity, the parameter interval for both curves is normalized to  $[0, 1]$  in the following explanations. Denote the original curve by  $c_1 : [0, 1] \rightarrow \mathbb{R}^2$  and the offset curve by  $c_2$ . The quality test is passed if the offset curve fulfills at each of the 19 test points  $t_i \in \{\frac{1}{20}, \dots, \frac{19}{20}\}$  one of the following two conditions:

- Let  $v$  be the tangent vector  $c_1'(t_i)$ . For  $w := c_1(t_i) - c_2(t_i)$ , denote by  $w_{par}$  the component parallel to  $v$  and by  $w_{orth}$  the component orthogonal to  $v$ . The test is passed if  $|w_{par}| + |w_{orth} - \xP@off| \leq \frac{1}{8}\xP@maxdev$ . If  $\|v\|$  is very small so that the direction cannot be determined precisely, the condition is  $\|c_1(t_i) - c_2(t_i)\| - |\xP@off| \leq \frac{1}{8}\xP@maxdev$ .
- Compute the normal line at  $t_i$  to the curve  $c_1$  and intersect it with  $c_2$ . The intersection point is allowed to have a different parameter  $\tilde{t}_i \in [t_i - 0.5, t_i + 0.5] \cap [0, 1]$ . Then let  $w := c_1(t_i) - c_2(\tilde{t}_i)$  and test whether  $|w_{par}| + |w_{orth} - \xP@off| \leq \frac{1}{8}\xP@maxdev$ . ( $|w_{par}|$  is very small in this case and is nonzero only because of limited precision, in particular since  $\tilde{t}_i$  is determined with an error of  $\approx 2^{-17}$  ( $= \frac{1}{2}sp$ ).)

```
1108 \newcommand*\xP@testoffset{%
```

Default values for the return statement and the loop continuation.

```

1109   \gdef\@gtempa{\xP@offsetoktrue}%
1110   \def\@gtempb{\ifdim\xP@ti<1.85pt}%
1111   \xP@ti.1pt
1112   \loop

   \xP@tip =  $t_i$ , denormalized for  $c_1$ 
1113   \xP@tip
1114   \dimexpr\xP@a*131072/\xP@bigdim+(\xP@b-\xP@a)*\xP@ti/\xP@bigdim\relax

```

Point on the original curve  $c_1$  (scaled by  $-8$ )

```

1115   \L@p-\xP@bezierpoly\xP@xa\xP@xb\xP@xc\xP@xd\xP@tip
1116   \U@p-\xP@bezierpoly\xP@ya\xP@yb\xP@yc\xP@yd\xP@tip

```

$8c_2(t_i) - 8c_1(t_i)$

```

1117 \xP@valA\xP@bezierpoly\X@p\L@c\R@c\X@c\xP@ti
1118 \advance\xP@valA\L@p
1119 \xP@valB\xP@bezierpoly\Y@p\U@c\D@c\Y@c\xP@ti
1120 \advance\xP@valB\U@p
v
1121 \@tempdima\dimexpr\xP@tip/2\relax
1122 \xP@velocity@@
Decide if  $v$  is big enough (heuristically, may be changed in the future)
1123 \@tempdimc\dimexpr(\xP@b-\xP@a)*\@tempdimb/\xP@bigdim\relax
1124 \xP@abs\@tempdimc
1125 \ifdim.01pt<\@tempdimc
8 $w_{par}$ , 8 $w_{orth}$  - 8\xP@off,
1126 \xP@devA\dimexpr\xP@valA*\d@X/\@tempdimb+\xP@valB*\d@Y/\@tempdimb\relax
1127 \xP@devB\dimexpr\xP@valA*\d@Y/\@tempdimb-\xP@valB*\d@X/\@tempdimb-8\xP@off
1128 \relax
1129 \xP@abs\xP@devA
1130 \xP@abs\xP@devB
1131 \@tempdima\dimexpr\xP@devA+\xP@devB\relax
1132 \else
If the velocity is really too small, just pass the test.
1133 \ifdim.0005pt>\@tempdimc
1134 \@tempdima\z@
1135 \else
8|| $c_1(t_i) - c_2(t_i)$ ||
1136 {%
1137 \d@X\xP@valA
1138 \d@Y\xP@valB
1139 \xP@vecclen@
1140 \global\dimen@i\@tempdimb
1141 }\@tempdima\dimen@i
1142 \advance\@tempdima\ifdim\xP@off>\z@-\fi8\xP@off
1143 \xP@abs\@tempdima
1144 \fi
1145 %\@tempdima\z@
1146 \fi
If the first condition is not fulfilled, test the second one.
1147 \ifdim\@tempdima>\xP@maxdev
 $c_1(t_i)$ 
1148 \divide\L@p8\relax
1149 \divide\U@p8\relax
Affine transformation of the offset curve: translate by  $-c_1(t_i)$  and rotate so that the tangent
 $v$  to  $c_1(t_i)$  becomes the  $x$ -axis.
1150 {%
1151 \xP@transformcoor\X@p\Y@p
1152 \xP@transformcoor\L@c\U@c
1153 \xP@transformcoor\R@c\D@c
1154 \xP@transformcoor\X@c\Y@c
Find the parameter  $\tilde{t}_i$  and decide whether the approximation at  $\tilde{t}_i$  is good.
1155 \xP@findzero
1156 }%
1157 \fi
1158 \@gtempb
1159 \advance\xP@ti.1pt
1160 \repeat

```

```

1161 \expandafter}\@gtempa
1162 }

```

**\xP@transformcoor** •5 Affine coordinate transformation. First, translate the coordinates in (#1,#2) by the vector  $-(\text{\L@p}, \text{\U@p})$ , then rotate by the angle between  $v := (\text{\d@X}, \text{\d@Y})$  and  $(1,0)$ . The register `\@tempdimb` must contain the length  $\|v\|$ .

```

1163 \newcommand*\xP@transformcoor[2]{%
1164   \advance#1\L@p
1165   \advance#2\U@p
1166   \@tempdima\dimexpr#1*\d@X/\@tempdimb+#2*\d@Y/\@tempdimb\relax
1167   #2\dimexpr#2*\d@X/\@tempdimb-#1*\d@Y/\@tempdimb\relax
1168   #1\@tempdima
1169 }

```

**\xP@findzero** •5 Find the parameter  $\tilde{t}_i$  by nested intervals/intermediate value theorem.

```

1170 \newcommand*\xP@findzero{%
1171   \xP@setleftvalue\tw@
1172   \xP@setrightvalue\tw@

```

Normalize: function value ( $x$ -coordinate) should be nonnegative at the upper end.

```

1173   \ifdim\xP@valB<\z@\xP@reversecoeff\fi

```

If the function value at the lower end is also positive, try a smaller parameter interval  $t_i \pm \frac{1}{n}$  for  $n \in \{3, 4, 5, 7, 10, 20\}$ . Maybe we have different signs for the  $x$ -coordinate for the smaller boundary parameters.

```

1174   \ifdim\xP@valA>\z@
1175     \@tempswatrue
1176     \for\@tempa:={\thr@@,4,5,7,10,20}\do{%
1177       \if@tempswa
1178         \xP@setleftvalue\@tempa
1179         \ifdim\xP@valA<\z@\@tempswafalse\fi
1180         \if@tempswa
1181           \xP@setrightvalue\@tempa
1182           \ifdim\xP@valB<\z@
1183             \@tempswafalse
1184             \xP@reversecoeff
1185           \fi
1186         \fi
1187       \fi
1188     }%

```

Last resort: Try the midpoint.

```

1189   \if@tempswa
1190     \L@p\xP@ti
1191     \xP@valA\dimexpr\xP@bezierpoly\X@p\L@c\R@c\X@c\L@p\relax
1192     \ifdim\xP@valA>\z@
1193       \U@p\L@p
1194       \xP@valB\xP@valA
1195     \fi
1196   \fi
1197 \fi

```

The actual nested interval algorithm

```

1198 \loop
1199 \ifnum\numexpr\U@p-\L@p\relax>\@ne
1200   \xP@ti\dimexpr(\L@p+\U@p)/2\relax
1201   \xP@devA\xP@bezierpoly\X@p\L@c\R@c\X@c\xP@ti
1202   \ifdim\xP@devA>\z@
1203     \U@p\xP@ti
1204     \xP@valB\xP@devA
1205   \else
1206     \L@p\xP@ti

```

```

1207      \xP@valA\xP@devA
1208      \fi
1209  \repeat

```

Take the left or right boundary point (only 1sp apart), depending on which one yields the smaller  $x$ -coordinate.

```

1210  \xP@ifabsless\xP@valB\xP@valA
1211      \L@p\U@p
1212      \xP@valA\xP@valB
1213  \fi

  Compare the  $y$ -coordinate with \xP@off.

1214  \xP@valB\dimexpr\xP@bezierpoly\Y@p\U@c\D@c\Y@c\L@p+8\xP@off\relax
1215  \xP@abs\xP@valA
1216  \xP@abs\xP@valB
1217  \ifdim\dimexpr\xP@valA+\xP@valB\relax>\xP@maxdev
1218      \xP@failed
1219  \fi
1220 }

```

\xP@failed Break the loop for the  $t_i$  in \xP@testoffset. Set the return value to false.

```

1221 \newcommand*\xP@failed{%
1222   \global\let@gtempb\iffalse
1223   \gdef\@gtempa{\xP@offsetokfalse}%
1224 }

```

\xP@reversecoeff Reverse the function for the nested interval algorithm.

```

1225 \newcommand*\xP@reversecoeff{%
1226   \multiply\X@p\m@ne
1227   \multiply\L@c\m@ne
1228   \multiply\R@c\m@ne
1229   \multiply\X@c\m@ne
1230   \multiply\xP@valA\m@ne
1231   \multiply\xP@valB\m@ne
1232 }

```

\xP@setleftvalue •5

```

1233 \newcommand*\xP@setleftvalue[1]{%
1234   \L@p\dimexpr\xP@ti-\p@/#1\relax
1235   \ifdim\L@p<z@\L@p\z@\fi
1236   \xP@valA\dimexpr\xP@bezierpoly\X@p\L@c\R@c\X@c\L@p\relax
1237 }

```

\xP@setrightvalue •5

```

1238 \newcommand*\xP@setrightvalue[1]{%
1239   \U@p\dimexpr\xP@ti+\p@/#1\relax
1240   \ifdim\U@p>2\p@\U@p2\p@\fi
1241   \xP@valB\dimexpr\xP@bezierpoly\X@p\L@c\R@c\X@c\U@p\relax
1242 }

```

## 7.8 Multiple dashed curves

\xP@splinedbldashed

```

1243 \newcommand*\xP@splinedbldashed{%
1244   \xP@checkspline\xP@splinemultdashed\xP@doublestroke}

```

\xP@splinetrbldashed

```

1245 \newcommand*\xP@splinetrbldashed{%
1246   \xP@checkspline\xP@splinemultdashed\xP@trblstroke}

```

```

\xP@splinemultdashed
1247 \newcommand*\xP@splinemultdashed{%
  Expected dash number
1248 \@tempcnta\numexpr2*\numexpr(\@tempdimb+xydashl@)/(2*xydashl@)\relax-1\relax
1249 \ifnum\@tempcnta>\@ne
1250 \expandafter\xP@splinemultdashed@
1251 \else
  One dash: paint a solid line
1252 \expandafter\xP@splinemultsolid
1253 \fi
1254 }

```

**\xP@splinemultdashed@** ●1 ●7 Make a list of parameter pairs for the start and end point of a dash.

```

1255 \newcommand*\xP@splinemultdashed@[1]{%
1256 \xP@inibigdim
  Dash length
1257 \@tempdima\dimexpr\@tempdimb/\@tempcnta\relax
1258 \xP@temppar\z@
1259 \toks@{}%
1260 \@tempcnta\z@
1261 \loop
1262 \advance\@tempcnta\@ne
1263 \xP@append\toks@{\ifodd\@tempcnta\noexpand\xP@paintdash\fi
1264 \the\xP@temppar}}%
1265 \xP@oldpar\xP@temppar
1266 \xP@slide
1267 \ifdim\xP@temppar<\xP@bigdim
1268 \repeat

  The last position is kept as a scaling factor so that the last dot can be drawn at exactly the
  parameter 1. Use the last or the next-to-last position, depending on the parity of segments.
1269 \xP@lastpar
1270 \ifodd\@tempcnta
1271 \xP@temppar
1272 \xP@append\toks@{\the\xP@temppar}}%
1273 \else
1274 \xP@oldpar
1275 \fi

```

Convert the list of parameters to a list of PDF tokens.

```

1276 \@temptokena{}%
1277 \xP@setsolidpat
1278 \@for\@tempa:={#1}\do{\the\toks@}%
1279 \xP@stroke{\the\@temptokena}%
1280 }}

```

**\xP@paintdash** ●1 ●7

```

1281 \newcommand*\xP@paintdash[2]{%
1282 \xP@paintsolid{\dimexpr#1*\xP@bigdim/\xP@lastpar\relax}%
1283 {\dimexpr#2*\xP@bigdim/\xP@lastpar\relax}%
1284 }

```

## 7.9 Multiple dotted curves

```

\splinedbldotted@
\xP@splinedbldotted@
1285 \xP@hook{splinedbldotted@}
1286 \newcommand*\xP@splinedbldotted@{%
1287 \let\xP@normalmult\@ne
1288 \xP@check spline\xP@splinemultdotted\xP@doublestroke}

```

`\xP@splinetrbldotted`

```
1289 \newcommand*\xP@splinetrbldotted{%
1290   \let\xP@normalmult\tw@
1291   \xP@checkspline\xP@splinemultdotted\xP@trblstroke}
```

`\xP@multidottedpat` Dotted lines with multiple strokes are drawn in a different way from single-stroked lines. They are composed of many small, straight lines normal to the curve at every dot position. Hence, the dot pattern for multiple curves has dots which are spaced by the normal distance between strokes.

```
1292 \newcommand*\xP@multidottedpat{%
1293   \def\xP@pattern{2 J [0 \xP@dim{\xydashh@}]0 d }%
1294 }
```

`\xP@normalmult`

```
1295 \@ifdefinable\xP@normalmult\relax
```

`\xP@splinemultdotted` ●1 ●7

```
1296 \newcommand\xP@splinemultdotted[1]{\%
1297   \xP@inibigdim
   Expected dot distance (see the formula in \xP@setdottedpat)
1298   \@tempdima\dimexpr\@tempdimb/\numexpr\@tempdimb/131072+1\relax\relax
```

Make a list of dot positions on the spline segment.

```
1299   \xP@temppar\z@
1300   \toks@{}%
1301   \loop
1302     \xP@append\toks@{\noexpand\xP@paintdot{\the\xP@temppar}}%
1303     \xP@oldpar\xP@temppar
1304     \xP@slide
1305     \ifdim\xP@temppar<\xP@bigdim
1306     \repeat
```

The last position is kept as a scaling factor so that the last dot can be drawn at exactly the parameter 1. Use the last or the next-to-last position, depending on which is closer to 1.

```
1307   \xP@lastpar
1308   \ifdim\dimexpr\xP@bigdim-\xP@oldpar\relax<\dimexpr\xP@temppar%
1309     -\xP@bigdim\relax
1310     \xP@oldpar
1311   \else
1312     \xP@temppar
1313     \xP@append\toks@{\noexpand\xP@paintdot{\the\xP@temppar}}%
1314   \fi
```

Convert the list of parameters to a list of PDF tokens.

```
1315   \@temptokena{}%
1316   \the\toks@
```

Actually draw the points in the list.

```
1317   \xP@multidottedpat
1318   \xP@stroke{\the\@temptokena}%
1319 }
```

`\xP@slide` ●1 ●7 Slide along the Bézier segment by `\@tempdima`. Needs: Xy-pic spline parameter, current position parameter `\xP@temppar`, total spline length `\@tempdimb`.

```
1320 \newcommand*\xP@slide{%
1321   \xP@slide@
```

Return the new spline parameter after sliding.

```
1322   \global\dimen@i\xP@temppar
1323   }\xP@temppar\dimen@i
1324 }
```

\xP@slide@ ●1 ●7

1325 \newcommand\*\xP@slide@{%

Compute the velocity at two points, the starting point and an estimate for the end point (estimation based on the total spline length).

1326 \xP@velocity{\xP@temppar\*\p@/\xP@bigdim}\xP@tempvel

1327 \xP@velocity{(\xP@temppar+\xP@bigdim/\numexpr\@tempdimb%

1328 /131072+1\relax)\*\p@/\xP@bigdim}\xP@tempvel@

Use the average velocity to compute the parameter increment. If the parameter increment is too big (i. e. the velocity was very small), increment the parameter by at most .1\xP@bigdim, compute the true partial spline length and slide again.

1329 \ifdim\dimexpr\@tempdima\*1310720/(\xP@tempvel+\xP@tempvel@)\relax>\p@

1330 {%

1331 \dimen5\xP@temppar

1332 \advance\xP@temppar.1\xP@bigdim

1333 \dimen7\xP@temppar

1334 \xP@shaveprec{\dimen5}{\dimen7}%

1335 \xP@bezierlength

1336 \advance\@tempdima-\@tempdimb

1337 \expandafter}\expandafter\@tempdima\the\@tempdima\relax

1338 \advance\xP@temppar.1\xP@bigdim

1339 \expandafter\xP@slide@

1340 \else

1341 \advance\xP@temppar

1342 \dimexpr2\xP@bigdim\*\@tempdima/(\xP@tempvel+\xP@tempvel@)\relax

1343 \fi

1344 }

\xP@paintdot ●1 ●7

1345 \newcommand\*\xP@paintdot[1]{%

Scale the parameter with a correction factor

1346 \xP@temppar\dimexpr#1\*\xP@bigdim/\xP@lastpar\relax

Auxiliary variables

1347 \L@p\dimexpr\L@c-\X@p\relax

1348 \D@p\dimexpr\U@c-\Y@p\relax

Velocity vector at parameter value \xP@temppar

1349 \d@X3\dimexpr((\X@c-\X@p+(\L@c-\R@c)\*3)\*\xP@temppar/\xP@bigdim

1350 +(\R@c-\L@p-\L@c)\*2)\*\xP@temppar/\xP@bigdim+\L@p\relax

1351 \d@Y3\dimexpr((\Y@c-\Y@p+(\U@c-\D@c)\*3)\*\xP@temppar/\xP@bigdim

1352 +(\D@c-\D@p-\U@c)\*2)\*\xP@temppar/\xP@bigdim+\D@p\relax

1353 \xP@vecLen

If the velocity is zero, use its first derivative instead to obtain the direction (up to a factor of 6).

1354 \ifdim\@tempdimb=\z@

1355 \d@X3\dimexpr(\X@c-\X@p+(\L@c-\R@c)\*3)\*\xP@temppar/\xP@bigdim

1356 +(\R@c-\L@p-\L@c)\relax

1357 \d@Y3\dimexpr(\Y@c-\Y@p+(\U@c-\D@c)\*3)\*\xP@temppar/\xP@bigdim

1358 +(\D@c-\D@p-\U@c)\relax

1359 \xP@vecLen

If the first derivative is zero, take the second one (again up to a factor of 6).

1360 \ifdim\@tempdimb=\z@

1361 \d@X3\dimexpr\X@c-\X@p+(\L@c-\R@c)\*3\relax

1362 \d@Y3\dimexpr\Y@c-\Y@p+(\U@c-\D@c)\*3\relax

1363 \xP@vecLen

1364 \fi

1365 \fi

Position at parameter value \xP@temppar

```

1366 \U@p\dimexpr\R@c-\L@p-\L@c\relax
1367 \R@p\dimexpr\X@c-3\R@c+3\L@c-\X@p\relax
1368 \X@min\dimexpr\D@c-\D@p-\U@c\relax
1369 \Y@min\dimexpr\Y@c-3\D@c+3\U@c-\Y@p\relax
1370 \xP@posX\dimexpr\X@p+(3\L@p+(3\U@p+\R@p*\xP@temppar/\xP@bigdim)%
1371      *\xP@temppar/\xP@bigdim)*\xP@temppar/\xP@bigdim\relax
1372 \xP@posY\dimexpr\Y@p+(3\D@p+(3\X@min+\Y@min*\xP@temppar/\xP@bigdim)%
1373      *\xP@temppar/\xP@bigdim)*\xP@temppar/\xP@bigdim\relax

```

Normal vector to the curve with length \xydashhh@

```

1374 \L@p\dimexpr\xydashhh@*\d@Y/\@tempdimb/2\relax
1375 \U@p\dimexpr-\xydashhh@*\d@X/\@tempdimb/2\relax

```

Append two points on both sides of the curve to the list. (The “zerodot” pattern is made to draw points with distance \xydashhh@.)

```

1376 \xP@append\@temptokena{\xP@coor{\xP@posX+\L@p*\xP@normalmult}%
1377      {\xP@posY+\U@p*\xP@normalmult}m %
1378 \xP@coor{\xP@posX-\L@p*(\xP@normalmult+\@ne)}%
1379      {\xP@posY-\U@p*(\xP@normalmult+\@ne)}l }%
1380 }

```

## 7.10 Squiggled curves

\xP@splinesquiggled

```

1381 \newcommand*\xP@splinesquiggled{%
1382 \xP@checkspline\xP@splinesquiggled@z@}

```

\xP@splinedblsquiggled

```

1383 \newcommand*\xP@splinedblsquiggled{%
1384 \xP@checkspline\xP@splinesquiggled@\xP@doublestroke}

```

\xP@splinetrbldsquiggled

```

1385 \newcommand*\xP@splinetrbldsquiggled{%
1386 \xP@checkspline\xP@splinesquiggled@\xP@trblstroke}

```

\xP@splinesquiggled@ ● 1 ● 7

```

1387 \newcommand*\xP@splinesquiggled@[1]{{%
1388 \xP@inibigdim

```

Expected squiggle length

```

1389 \@tempcnta=\numexpr\@tempdimb/\xybsql1@ \relax
1390 \ifnum\@tempcnta<\tw@\@tempcnta\tw@\fi
1391 \multiply\@tempcnta\tw@
1392 \@tempdima\dimexpr\@tempdimb/\@tempcnta \relax

```

Make a list of dot positions on the spline segment.

```

1393 \xP@temppar\z@
1394 \toks@{}%
1395 \@tempcnta\z@
1396 \loop
1397 \advance\@tempcnta\@ne
1398 \xP@append\toks@{\noexpand\xP@paintsquiggle{\the\xP@temppar}}%
1399 \xP@oldpar\xP@temppar
1400 \xP@slide
1401 \ifdim\xP@temppar<\xP@bigdim
1402 \repeat

```

The last position is kept as a scaling factor so that the last dot can be drawn at exactly the parameter 1. Use the last or the next-to-last position, on the parity of the number of positions.

```

1403 \xP@lastpar

```



```

1404     \ifodd\@tempcnta
1405     \xP@oldpar
1406     \else
1407     \xP@temppar
1408     \xP@append\toks@{\noexpand\xP@paintsquiggle{\the\xP@temppar}}}%
1409     \fi

```

Convert the list of parameters to a list of PDF tokens.

```

1410     \@temptokena{}%
1411     \xP@setsolidpat
1412     \@for\@tempa:={#1}\do{%
1413         \let\xP@dosquiggle\xP@dosquiggle@
1414         \count@\z@
1415         \the\toks@
1416     }%
1417     \xP@stroke{\the\@temptokena}
1418 }}

```

\xP@paintsquiggle ●1 ●7

```

1419 \newcommand*\xP@paintsquiggle[1]{%
    Scale the parameter with a correction factor
1420 \xP@temppar\dimexpr#1*\xP@bigdim/\xP@lastpar\relax
    Auxiliary variables
1421 \L@p\dimexpr\L@c-\X@p\relax
1422 \D@p\dimexpr\U@c-\Y@p\relax
    Velocity vector at parameter value \xP@temppar
1423 \d@X3\dimexpr((\X@c-\X@p+(\L@c-\R@c)*3)*\xP@temppar/\xP@bigdim
1424 +(\R@c-\L@p-\L@c)*2)*\xP@temppar/\xP@bigdim+\L@p\relax
1425 \d@Y3\dimexpr((\Y@c-\Y@p+(\U@c-\D@c)*3)*\xP@temppar/\xP@bigdim
1426 +(\D@c-\D@p-\U@c)*2)*\xP@temppar/\xP@bigdim+\D@p\relax
1427 \xP@vecLen

```

If the velocity is zero, take its first derivative instead to obtain the direction (up to a factor of 6).

```

1428 \ifdim\@tempdimb=\z@
1429 \d@X3\dimexpr(\X@c-\X@p+(\L@c-\R@c)*3)*\xP@temppar/\xP@bigdim
1430 +(\R@c-\L@p-\L@c)\relax
1431 \d@Y3\dimexpr(\Y@c-\Y@p+(\U@c-\D@c)*3)*\xP@temppar/\xP@bigdim
1432 +(\D@c-\D@p-\U@c)\relax
1433 \xP@vecLen

```

If the first derivative is zero, take the second one (again up to a factor of 6).

```

1434 \ifdim\@tempdimb=\z@
1435 \d@X3\dimexpr\X@c-\X@p+(\L@c-\R@c)*3\relax
1436 \d@Y3\dimexpr\Y@c-\Y@p+(\U@c-\D@c)*3\relax
1437 \xP@vecLen
1438 \fi
1439 \fi

```

Position at parameter value \xP@temppar

```

1440 \U@p\dimexpr\R@c-\L@p-\L@c\relax
1441 \R@p\dimexpr\X@c-3\R@c+3\L@c-\X@p\relax
1442 \X@min\dimexpr\D@c-\D@p-\U@c\relax
1443 \Y@min\dimexpr\Y@c-3\D@c+3\U@c-\Y@p\relax
1444 \xP@posX\dimexpr\X@p+(3\L@p+(3\U@p+\R@p*\xP@temppar/\xP@bigdim)%
1445 *\xP@temppar/\xP@bigdim)*\xP@temppar/\xP@bigdim\relax
1446 \xP@posY\dimexpr\Y@p+(3\D@p+(3\X@min+\Y@min*\xP@temppar/\xP@bigdim)%
1447 *\xP@temppar/\xP@bigdim)*\xP@temppar/\xP@bigdim\relax

```

Offset to the current position for multiple curves.

```

1448 \advance\xP@posX\dimexpr-\d@Y*\numexpr\@tempa\relax/\@tempdimb\relax
1449 \advance\xP@posY\dimexpr\d@X*\numexpr\@tempa\relax/\@tempdimb\relax

```

Tangent vector to the curve with correct length

```

1450 \L@p\dimexpr\d@X*\@tempdima/\@tempdimb\relax
1451 \U@p\dimexpr\d@Y*\@tempdima/\@tempdimb\relax
1452 \R@p\dimexpr\L@p*543339720/1311738121\relax
1453 \D@p\dimexpr\U@p*543339720/1311738121\relax
1454 \X@min\dimexpr\L@p*362911648/967576667\relax
1455 \Y@min\dimexpr\U@p*362911648/967576667\relax
1456 \X@max\dimexpr(\L@p+\U@p)*173517671/654249180\relax
1457 \Y@max\dimexpr(\L@p-\U@p)*173517671/654249180\relax

1458 \xP@dosquiggle
1459 \ifnum\count@=\thr@@\relax\count@\z@ \else\advance\count@\@ne\fi
1460 }

```

\xP@dosquiggle •7

```

1461 \@ifdefinable\xP@dosquiggle@\relax

```

\xP@dosquiggle@ •7

```

1462 \newcommand*\xP@dosquiggle@{%
1463   \edef\next@{\xP@coor{\xP@posX}{\xP@posY}m %
1464     \xP@coor{\xP@posX+\Y@max}{\xP@posY+\X@max}%
1465   }%
1466   \let\xP@dosquiggle\xP@dosquiggle@@
1467 }

```

\xP@dosquiggle@@ •7

```

1468 \newcommand*\xP@dosquiggle@@{%
1469   \xP@append\@temptokena{\next@\expandafter\xP@coor
1470     \ifcase\count@
1471       {\xP@posX-\Y@max}{\xP@posY-\X@max}%
1472       \xP@coor\xP@posX\xP@posY
1473     \or
1474       {\xP@posX-\D@p-\X@min}{\xP@posY+\R@p-\Y@min}%
1475       \xP@coor{\xP@posX-\D@p}{\xP@posY+\R@p}%
1476     \or
1477       {\xP@posX-\X@max}{\xP@posY+\Y@max}%
1478       \xP@coor\xP@posX\xP@posY
1479     \or
1480       {\xP@posX+\D@p-\X@min}{\xP@posY-\R@p-\Y@min}%
1481       \xP@coor{\xP@posX+\D@p}{\xP@posY-\R@p}%
1482     \fi c }%
1483   \edef\next@{\expandafter\xP@coor
1484     \ifcase\count@
1485       {\xP@posX+\Y@max}{\xP@posY+\X@max}%
1486     \or
1487       {\xP@posX-\D@p+\X@min}{\xP@posY+\R@p+\Y@min}%
1488     \or
1489       {\xP@posX+\X@max}{\xP@posY-\Y@max}%
1490     \or
1491       {\xP@posX+\D@p+\X@min}{\xP@posY-\R@p+\Y@min}%
1492     \fi
1493   }%
1494 }

```

## 7.11 Circles

\circhar@@ Replacement macro for the circle chars.

```

\xP@circhar@@ 1495 \xP@hook{circhar@@}
1496 \newcommand*\xP@circhar@@[1]{%
1497   \expandafter\xP@circhar@@@\ifcase#1 %

```

Bézier segments for  $1/8$  circle. Let

$$\begin{aligned} a &:= \sqrt{1/2} \approx .707106781, \\ b &:= \frac{8}{3}\sqrt{2}\cos(\pi/8)(1 - \cos(\pi/8)) \approx .2652164898, \\ c &:= \frac{1}{3}(-3 + 8\cos(\pi/8) - 2\cos^2(\pi/8)) \approx .8946431596, \\ d &:= \frac{1}{2}b(2 + 3\cos(\pi/8) - \cos^2(\pi/8)) \approx .5195704027. \end{aligned}$$

(We have  $\cos(\pi/8) = \frac{1}{2}\sqrt{2 + \sqrt{2}}$ .)

The fractions below are best possible rational approximations (obtained by continued fractions) to the following coordinates:

$$(0, 0), (0, -b), (1 - c, -d), (1 - a, a)$$

```

1498      00%
1499      0{-173517671/654249180}%
1500      {65307479/619869377}{-34221476/65864945}%
1501      {225058681/768398401}{-543339720/768398401}%
1502      \or
      (0, -a), (a - d, -c), (a - b, -1), (a, -1)
1503      0{-543339720/768398401}%
1504      {181455824/967576667}{-554561898/619869377}%
1505      {826676217/1870772527}{-1}%
1506      {543339720/768398401}{-1}%
1507      \or
      (0, -1), (b, -1), (d, -c), (a, -a)
1508      0{-1}%
1509      {173517671/654249180}{-1}%
1510      {34221476/65864945}{-554561898/619869377}%
1511      {543339720/768398401}{-543339720/768398401}%
1512      \or
      (0, -a), (c - a, -d), (1 - a, -b), (1 - a, 0)
1513      0{-543339720/768398401}%
1514      {181455824/967576667}{-34221476/65864945}%
1515      {225058681/768398401}{-173517671/654249180}%
1516      {225058681/768398401}0%
1517      \or
      (0, a), (c - a, d), (1 - a, b), (1 - a, 0)
1518      0{543339720/768398401}%
1519      {181455824/967576667}{34221476/65864945}%
1520      {225058681/768398401}{173517671/654249180}%
1521      {225058681/768398401}0%
1522      \or
      (0, 1), (b, 1), (d, c), (a, a)
1523      01%
1524      {173517671/654249180}1%
1525      {34221476/65864945}{554561898/619869377}%
1526      {543339720/768398401}{543339720/768398401}%
1527      \or
      (0, a), (a - d, c), (a - b, 1), (a, 1)
1528      0{543339720/768398401}%
1529      {181455824/967576667}{554561898/619869377}%
1530      {826676217/1870772527}1%
1531      {543339720/768398401}1%
1532      \or
      (0, 0), (0, b), (1 - c, d), (1 - a, a)
1533      00%
1534      0{173517671/654249180}%

```

```

1535     {65307479/619869377}{34221476/65864945}%
1536     {225058681/768398401}{543339720/768398401}%
1537     \fi}

```

`\xP@circhar@@@` Draw the arc of  $1/8$  circle and use the same space as the chars from the circle font do.

```

1538 \newcommand\xP@circhar@@@[8]{%
1539   \xP@setsolidpat
1540   \xP@stroke{\xP@coord{\R@*#1}{\R@*#2}m
1541   \xP@coord{\R@*#3}{\R@*#4}\xP@coord{\R@*#5}{\R@*#6}%
1542   \xP@coord{\R@*#7}{\R@*#8}c}%
1543   \vrule width\z@ height\R@ depth\R@
1544   \kern\dimexpr\R@*#7\relax
1545 }

```

`\cirrestrict@@` Basically, `\cirrestrict@@` is turned into a no-op and does not change the radius.

```

\xP@cirrestrict@@ 1546 \xP@hook{cirrestrict@@}
1547 \newcommand*\xP@cirrestrict@@{\count@\z@\relax}

```